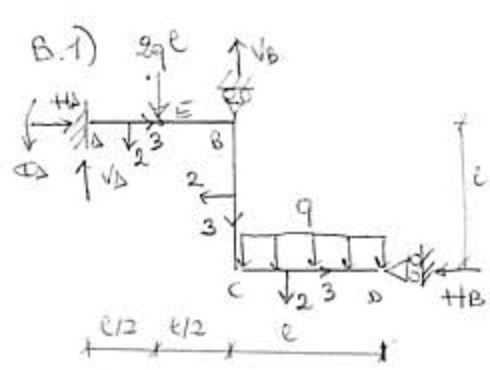


$$l_1 = 0.5 \text{ m}, l_2 = 1 \text{ m}, q = 1.5 \text{ t/m}, P = 3 \text{ t},$$
$$\sigma_{AMM} = 2400 \text{ kg/cm}^2, E = 2.1 \cdot 10^6 \text{ kg/cm}^2$$
$$\delta = 1 \text{ cm}$$

La travatura iperstatica di figura è realizzata con profilati IPE.

1. Utilizzando il metodo delle forze risolvere la travatura in presenza dei carichi q , P e disegnare i diagrammi delle caratteristiche di sollecitazione (N , T , M). Considerare trascurabili le deformazioni assiali.
2. Progettare la travatura.
3. Calcolare la rotazione del nodo B .
4. Risolvere nuovamente la travatura considerando anche il cedimento verticale δ del vincolo in B . Disegnare i nuovi diagrammi delle caratteristiche di sollecitazione (N , T , M) comprensivi sia di q , P che di δ .

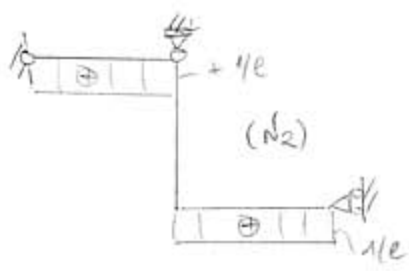
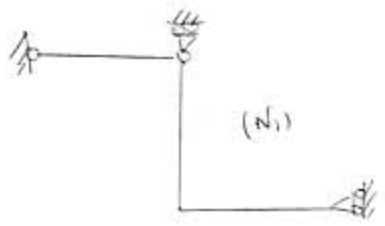
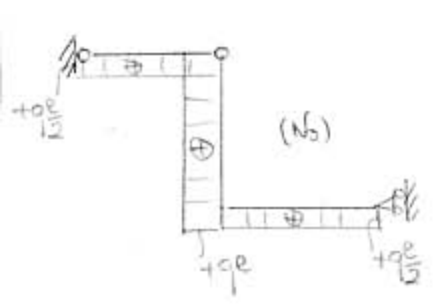
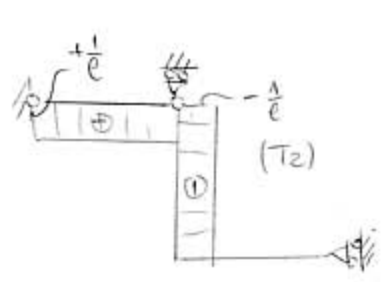
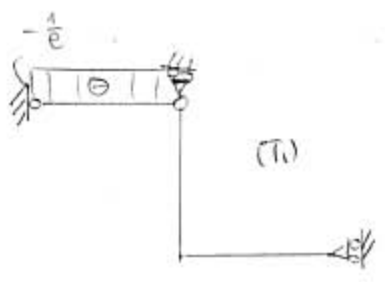
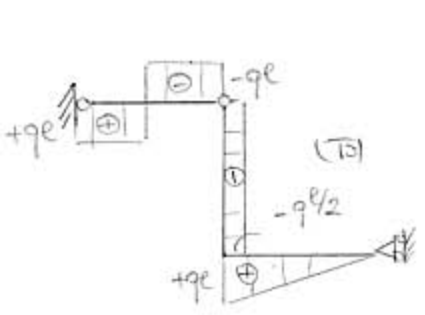
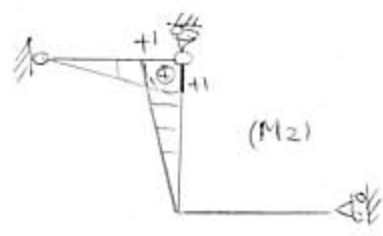
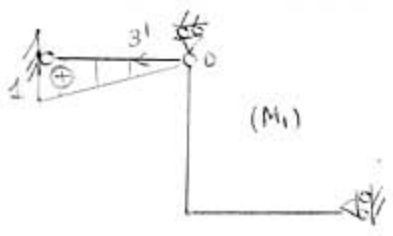
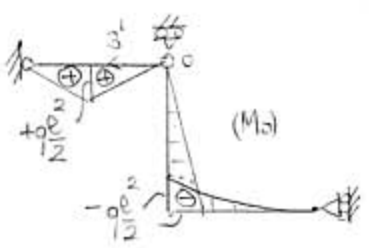
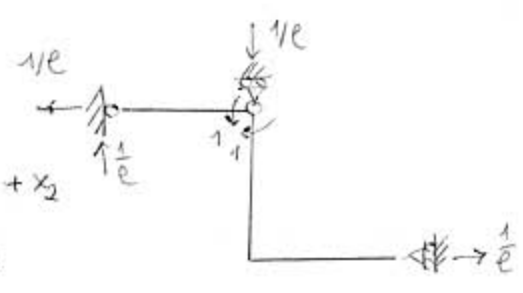
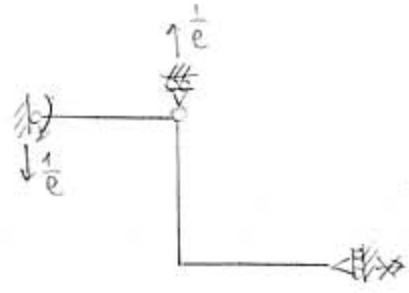
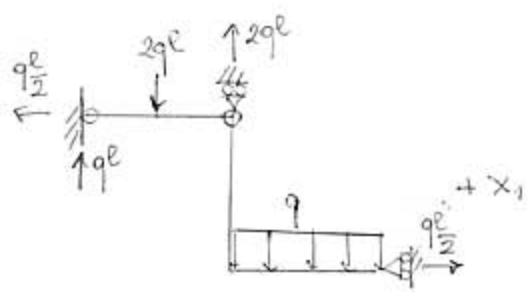


$$\rightarrow) H_2 = H_B$$

$$\uparrow) V_2 + V_B = qe + 2qe$$

$$\curvearrowright) \Delta_2 + V_B e - H_B e = 2qe \frac{e}{2} + qe \frac{3e}{2}$$

Trägertypus ohne feste iperstatische: Involgarise iperstatische: $X_1 = M_A$
 $X_2 = M_B$



$$EI_1 \gamma_{10} = \int_0^{e/2} (qe/x_3') \left(\frac{x_3'}{e} \right) dx_3' + \int_{e/2}^e (qe - qx_3') \left(\frac{x_3'}{e} \right) dx_3' = \frac{q}{3} \frac{e^3}{8} + q \left[\frac{2x_3'^2}{2} - \frac{x_3'^3}{3} \right]_{e/2}^e$$

$$= \frac{qe^3}{24} + q \left[\frac{e^3}{2} - \frac{e^3}{3} - \frac{e^3}{8} + \frac{e^3}{24} \right]$$

$$= \frac{qe^3}{24} + qe^3 \frac{(12 - 8 - 3 + 1)}{24}$$

$$= \frac{qe^3}{24} + \frac{qe^3}{12} = \frac{3}{24} qe^3 = \frac{qe^3}{8}$$

$$EI y_{20} = q \frac{e^3}{8} - \frac{1}{6} e \cdot 1 \cdot q \frac{e^2}{2} = q e^3 \left(\frac{1}{8} - \frac{1}{12} \right) = \frac{q e^3}{24}$$

$$EI y_{11} = \frac{e}{3}$$

$$EI y_{12} = \frac{e}{6}$$

$$EI y_{22} = \frac{2}{3} e$$

$$\begin{bmatrix} 4/3 & e/6 \\ e/6 & \frac{2}{3} e \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = -\frac{q e^3}{24} \begin{bmatrix} 3 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} 2 & 1 \\ 1 & 4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = -\frac{q e^2}{4} \begin{bmatrix} 3 \\ 1 \end{bmatrix} \rightarrow \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = -\frac{q e^2}{28} \begin{bmatrix} 4 & -1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} 3 \\ 1 \end{bmatrix}$$

$$= -\frac{q e^2}{28} \begin{bmatrix} 12-1 \\ -3+2 \end{bmatrix} = \begin{bmatrix} -\frac{11}{28} q e^2 \\ \frac{q e^2}{28} \end{bmatrix}$$

$$\det = 8 - 1 = 7$$

$$\begin{cases} x_1 = -\frac{11}{28} q e^2 = -589 \text{ kgm} \\ x_2 = \frac{q e^2}{28} = 54 \text{ kgm} \end{cases}$$

$$M_E = q \frac{e^2}{2} + \frac{x_1}{2} + \frac{x_2}{2} = q \frac{e^2}{2} - \frac{11}{56} q e^2 + \frac{1}{56} q e^2 = q e^2 \left(\frac{1}{2} - \frac{10}{56} \right) = \frac{9}{28} q e^2 = 482 \text{ kgm}$$

$$T_A = q e - \frac{x_1}{e} + \frac{x_2}{e} = 1500 + 589 + 54 = 2143 \text{ kg}$$

$$T_B = -q e - \frac{x_1}{e} + \frac{x_2}{e} = -1500 + 589 + 54 = -857 \text{ kg}$$

$$T_B^+ = -q \frac{e}{2} - \frac{x_2}{e} = -1500 - 54 = -1554 \text{ kg} = -\frac{q e^{1.5}}{2.14} \frac{q e}{28} = -\frac{15}{28} q e$$

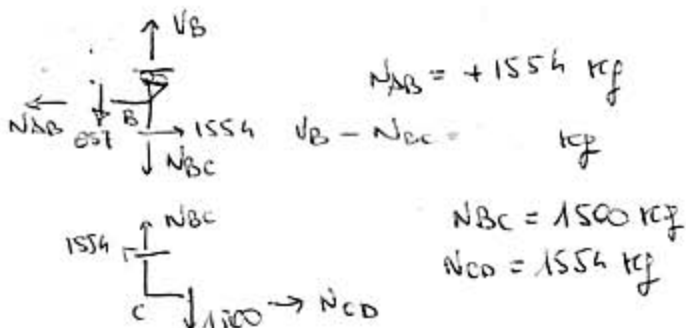


Diagramm:

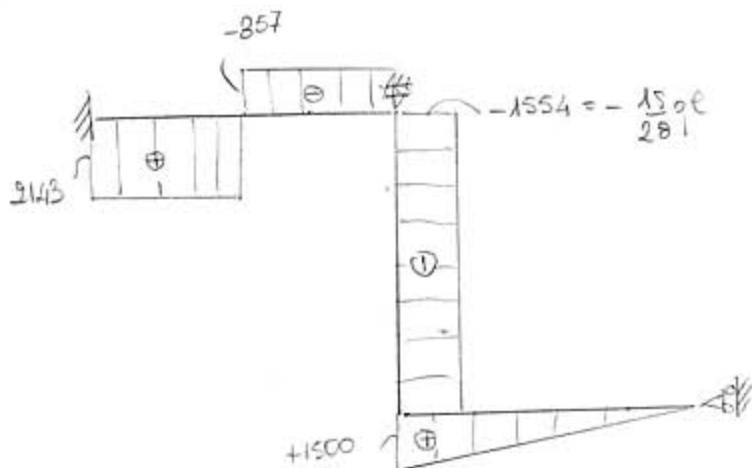
$$-\frac{11}{28} q l^2 = -582$$

$$\frac{9}{28} q l^2 = 482$$

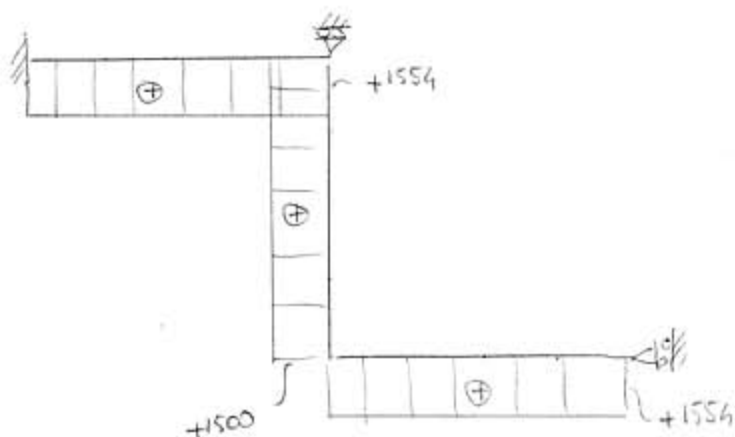
$$\frac{q l^2}{28} = 54$$

$$750 = q \frac{l^2}{2}$$

(M)
(kgm)



(T)
(kg)



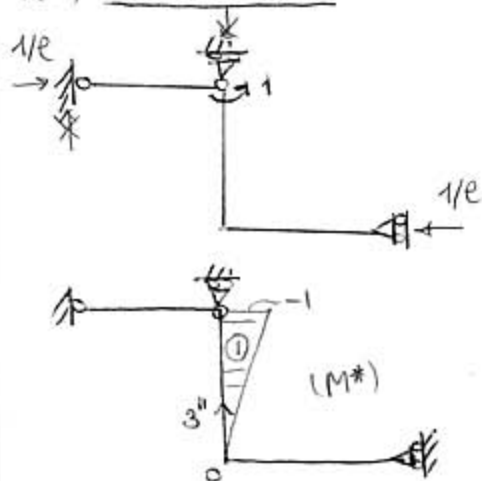
(N)
(kg)

B.2) Projektor: $N_1 \geq \frac{750 \cdot 140}{2400} = 31,2 \text{ cm}^3 \rightarrow \text{IPE } 80$

$$I_1 = 80 \text{ cm}^4$$

$$A = 7,6 \text{ cm}^2$$

B.3) Rotations w B



$$1 \cdot \varphi_B = \frac{1}{EI_1} \int_0^l \left(-\frac{x_3^2}{2} \right) \left(-q \frac{l^2}{2} + \frac{15}{28} q l x_3' \right) dx_3'$$

$$= \frac{1}{EI_1} \int_0^l \left(\frac{15}{28} q x_3'^2 + q \frac{l^2}{2} x_3' \right) dx_3'$$

$$= \frac{1}{EI_1} \left[-\frac{15}{28} q \frac{l^3}{3} + q \frac{l^3}{4} \right] = \frac{1}{EI_1} \frac{(-15+21)}{84} q l^3 = \frac{q l^3}{14 EI_1}$$

$$= \frac{15 \cdot 140^3}{14 \cdot 2,1 \cdot 10^6 \cdot 80} = 0,36^\circ$$

B.4) Cedimento

$$\begin{cases} \gamma_1 = \gamma_{10} + \gamma_{11} X_1 + \gamma_{12} X_2 & \gamma_1 = -\delta/e \\ \gamma_2 = \gamma_{20} + \gamma_{21} X_1 + \gamma_{22} X_2 & \gamma_2 = \delta/e \end{cases}$$

$$\begin{bmatrix} e/3 & e/6 \\ e/6 & 2/3 e \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = -\frac{qe^3}{24} \begin{bmatrix} 3 \\ 1 \end{bmatrix} + \frac{EI_1 \delta}{e} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} 2 & 1 \\ 1 & 4 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = -\frac{qe^2}{4} \begin{bmatrix} 3 \\ 1 \end{bmatrix} + \frac{6EI_1 \delta}{e^2} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

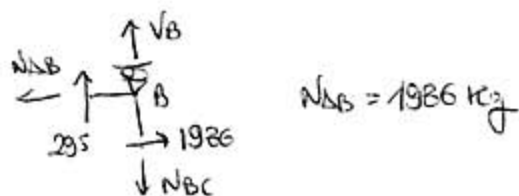
$$\begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} -\frac{11}{28} qe^2 \\ \frac{qe^2}{28} \end{bmatrix} + \frac{6}{7} \frac{EI_1 \delta}{e^2} \begin{bmatrix} 4 & -1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix} = \begin{bmatrix} -\frac{11}{28} qe^2 - \frac{30}{7} \frac{EI_1 \delta}{e^2} \\ \frac{qe^2}{28} + \frac{18}{7} \frac{EI_1 \delta}{e^2} \end{bmatrix}$$

$$\begin{cases} X_1 = -589 - \frac{30}{7} \frac{2,1 \cdot 10^6 \cdot 80 \cdot 1}{100} \frac{1}{100} = -589 - 720 = -1309 \text{ kgm} \\ X_2 = 54 + \frac{18}{7} \frac{2,1 \cdot 10^6 \cdot 80 \cdot 1}{100} \frac{1}{100} = 54 + 432 = 486 \text{ kgm} \end{cases}$$

$$M_E = qe^2 + \frac{X_1}{2} + \frac{X_2}{2} = 338 \text{ kgm}$$

$$T_A = 1500 + 1309 + 486 = 3295 \text{ kg}$$

$$T_B = -1500 + 1309 + 486 = 295$$



$$N_{AB} = 1926 \text{ kg}$$



$$N_{CD} = 1926 \text{ kg}$$

$$N_{CA} = 1500 \text{ kg}$$

Diagramm (couplem de q, P, δ):

