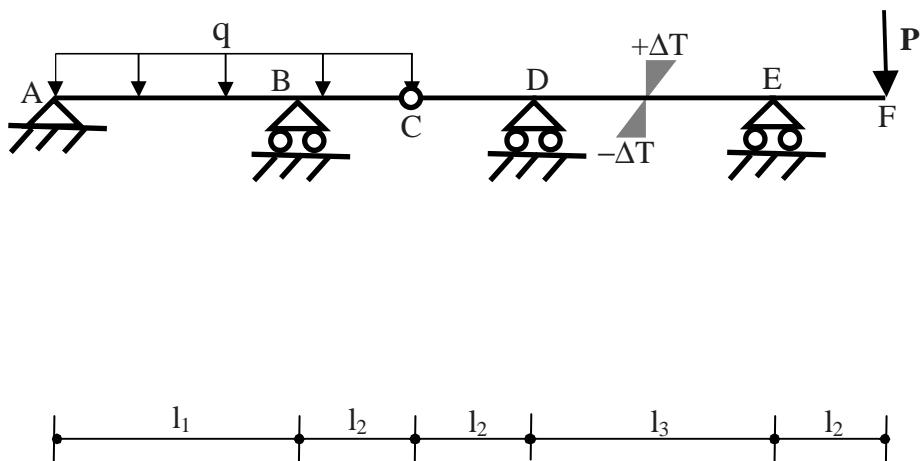


**CORSO DI LAUREA IN INGEGNERIA MECCANICA
UNIVERSITÀ DEGLI STUDI DI FERRARA
SECONDA PROVA SCRITTA PARZIALE DI STATICÀ
FERRARA, 24/11/2009**

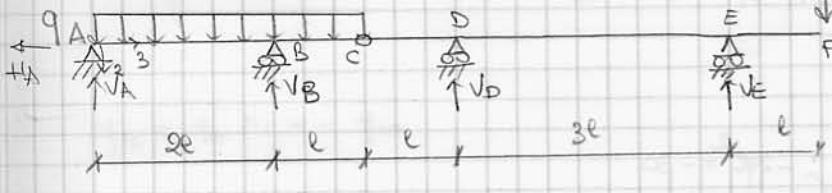


$$\begin{aligned}
 l_1 &= 2 \text{ m}, l_2 = 1 \text{ m}, l_3 = 3 \text{ m}, \\
 q &= 15 \text{ kN/m}, P = 30 \text{ kN}, \\
 E &= 2.1 \cdot 10^3 \text{ kN/cm}^2, \alpha = 10^{-5} \text{ }^\circ\text{C}^{-1}, \Delta T = 20 \text{ }^\circ\text{C}
 \end{aligned}$$

La travatura iperstatica di figura è realizzata con profilati IPE 200 ($H = 200 \text{ mm}$, $A = 28.4 \text{ cm}^2$, $I_1 = 1943 \text{ cm}^4$).

1. Utilizzando il metodo delle forze risolvere la travatura in presenza dei soli carichi q e P e disegnare i diagrammi delle caratteristiche della sollecitazione (N , T , M).
2. Calcolare la rotazione del nodo D.
3. Risolvere nuovamente la travatura considerando anche il carico termico nel solo tratto DE e disegnare i diagrammi delle caratteristiche della sollecitazione (N , T , M) comprensivi sia di q , P che di ΔT .

A1)



$$q = 15 \text{ kN/m}$$

$$l = 1 \text{ m}, \quad P = 30 \text{ kN} = 2ql$$

$$\begin{cases} H_A = 0 \\ V_A + V_B + V_D + V_E = 5ql \\ (C')_{ABC} V_A 3l + V_B l = \frac{9}{2} ql^2 \\ (C')_{CDE} V_D l + V_E l = 10ql^2 \end{cases}$$

$$H_A = 0$$

$$V_B = \frac{9}{2} ql - 3V_A$$

$$V_D = 10ql - 4V_E$$

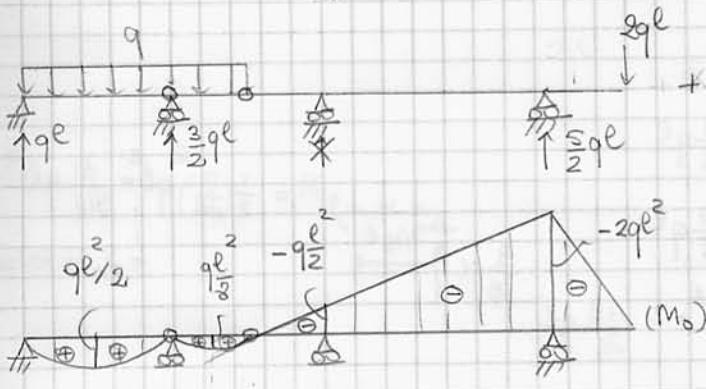
$$V_A + \frac{9}{2} ql - 3V_A + 10ql - 4V_E + V_E = 5ql$$

Trudniejsza i mniej wykonalna ipostaticzna.

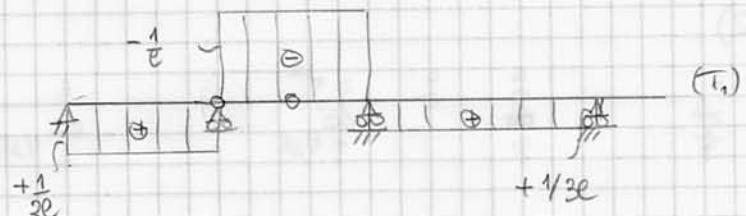
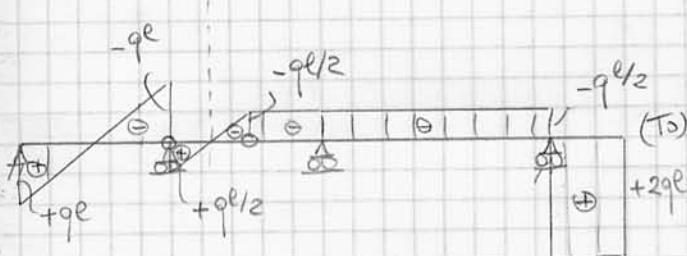
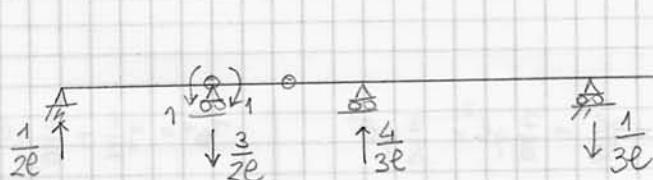
$$\text{Mucozymta ipostaticzna: } X_1 = M_B$$

$$\begin{cases} H_A = 0 \\ V_B = \frac{9}{2} ql - 3V_A \\ V_D = 10ql - \frac{38}{3} ql + \frac{8}{3} V_A = -\frac{8}{3} ql + \frac{8}{3} V_A \\ V_E = \frac{19}{6} ql - 2V_A \end{cases}$$

(0)



(1)



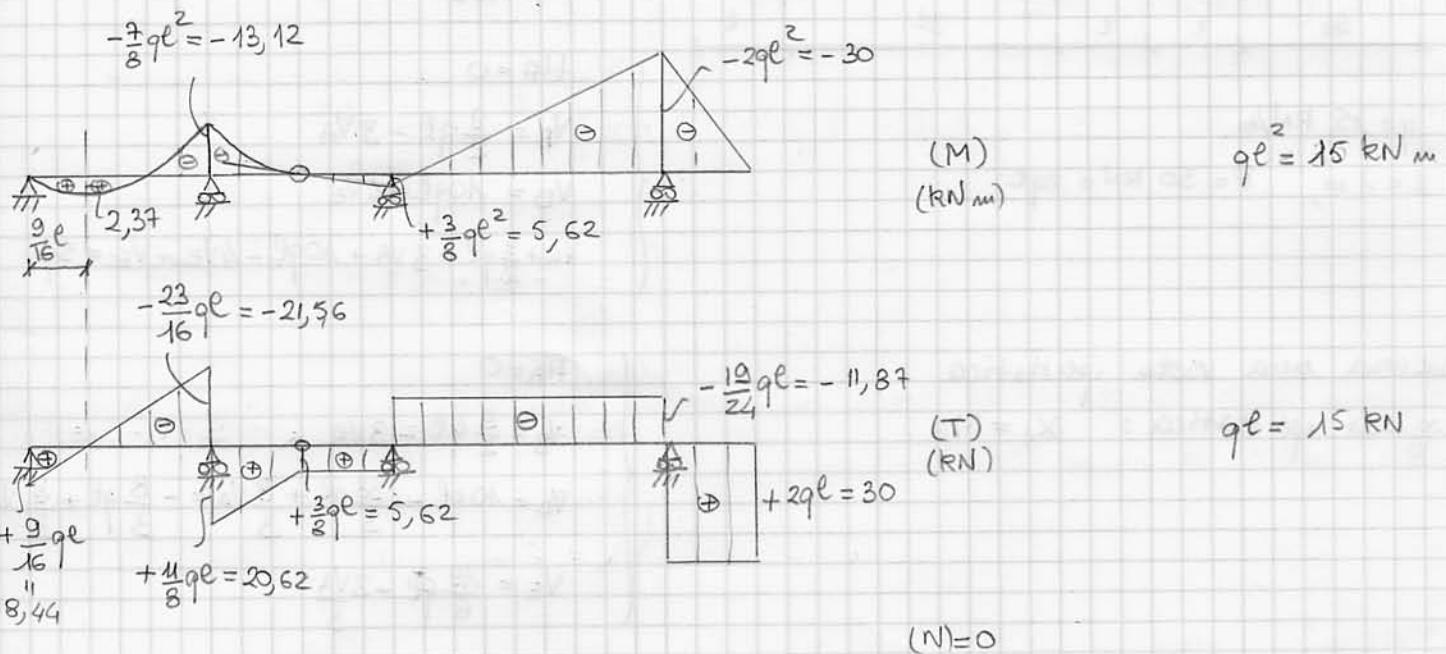
$$EI_1 M_{10} = \int_0^{2l} \left(\frac{x_3}{2e} \right) \left(qlx_3 - q \frac{x_3^2}{2} \right) dx_3 + \int_0^l \left(\frac{x_3}{e} \right) \left(q \frac{l}{2} x_3^2 - q \frac{x_3^2}{2} \right) dx_3 + \int_0^l \left(-q \frac{x_3'' l^2}{2} \right) \left(-\frac{x_3''}{e} \right) dx_3'' + \int_0^{3l} \left(-\frac{x_3'''}{e} \right) \left(-2ql^2 + q \frac{l}{2} x_3''' \right) dx_3'''$$

$$= qe^3/3 + qe^3/24 + qe^3/6 + \frac{3}{2} qe^3 = 49/24 qe^3$$

$$EI_1 M_{11} = \int_0^{2l} \left(\frac{x_3}{2e} \right)^2 dx_3 + 2 \int_0^l \left(\frac{x_3'}{e} \right)^2 dx_3' + \int_0^l \left(-\frac{x_3''}{e} \right)^2 dx_3'' = \frac{2l}{3} + \frac{2l}{3} + l = \frac{7}{3} l$$

$$X_1 = -\frac{49}{24} q \ell^3 \cdot \frac{3}{7\ell} = -\frac{7}{8} q \ell^2 = -13,12 \text{ kNm}$$

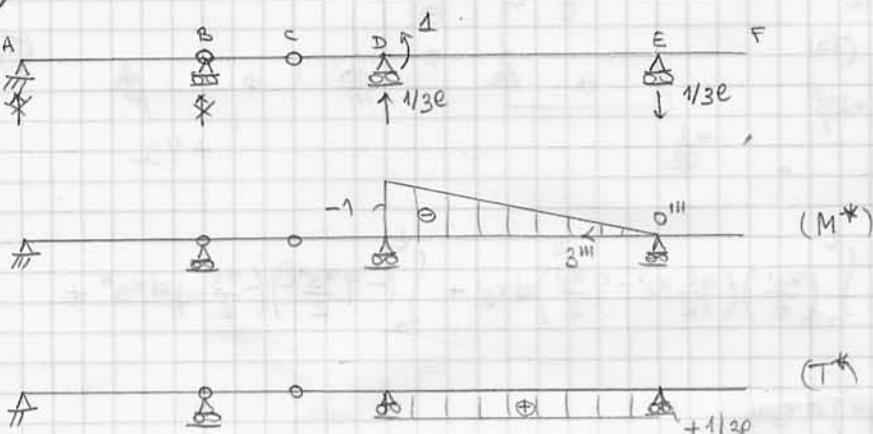
Diagramma delle c.s.:



Calcoli

$M_D = -q\ell^2 + \frac{7}{8}q\ell^2 = \frac{3}{8}q\ell^2$	$T_B^+ = q\ell + \frac{7}{8}q\ell = \frac{11}{8}q\ell$	$\bar{M} = \frac{1}{2}\left(\frac{9}{16}\right)q\ell^2 = \frac{81}{512}q\ell^2$
$T_A = q\ell - \frac{7}{16}q\ell = \frac{9}{16}q\ell$	$T_C = -q\ell + \frac{7}{8}q\ell = \frac{3}{8}q\ell$	$= 2,37 \text{ kNm}$
$T_B^- = -q\ell - \frac{7}{16}q\ell = -\frac{23}{16}q\ell$	$T_D^+ = -\frac{1}{38}\left(\frac{3}{8} + 2\right)q\ell^2 = -\frac{19}{24}q\ell$	

A2)



$$\Delta \varphi_D = \frac{1}{EI_1} \int_0^{3\ell} \left(-\frac{x_3'''}{3\ell} \right) \left(-2q\ell^2 + \frac{19}{24}q\ell x_3''' \right) dx_3''' = \frac{5q\ell^3}{8EI_1} = \frac{5 \cdot 15 \cdot 10^{-2} \cdot 100^3}{8 \cdot 21 \cdot 10^3 \cdot 1943} = 1,31^\circ$$

A3)

$$M_{1t} = \int_0^{3\ell} M_1 x_t \, dx_3 = X_t (-1) \frac{3\ell}{2} = \left(-\frac{8E\Delta T}{H} \right) \left(-\frac{3\ell}{2} \right) = +\frac{3\ell^2 \Delta T}{H}$$

$$M_{1t} + M_{11} x_1 = -M_{10}$$

$$X_1 = -\frac{M_{10}}{M_{11}} - \frac{M_{1t}}{M_{11}} = -\frac{\frac{7}{8}q\ell^2}{\frac{9EI_1}{2H}} - \frac{\frac{3\ell^2 \Delta TEI_1}{H}}{\frac{9EI_1}{2H}} = -\frac{\frac{7}{8}q\ell^2}{\frac{9EI_1}{2H}} \\ = (-13,12 - 0,026) \text{ KN m} \\ = -13,14 \text{ KN m}$$

I diagrammi delle caratteristiche delle reazioni non differiscono significativamente da quelli riportati al punto (1).