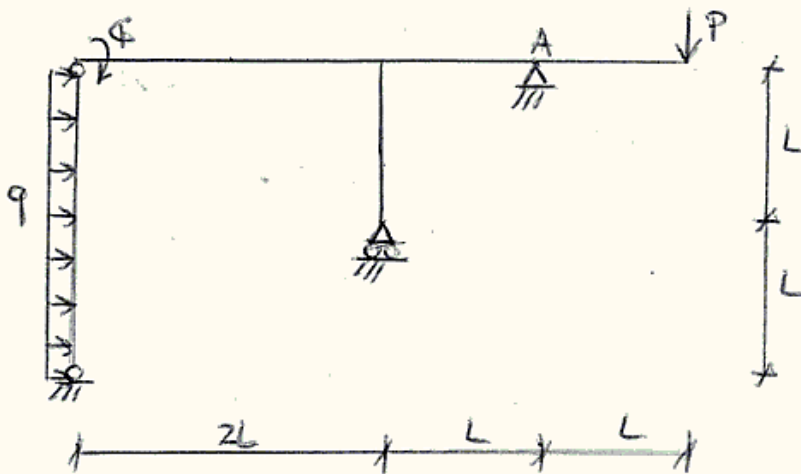


$L = 2 \text{ m}$, $q = 5 \text{ kN/m}$, $C = 20 \text{ kNm}$,
 $E = 210 \text{ GPa}$, $\alpha = 10^{-5} \text{ } ^\circ\text{C}^{-1}$

La travatura iperstatica di figura è realizzata con profilati IPE 160.

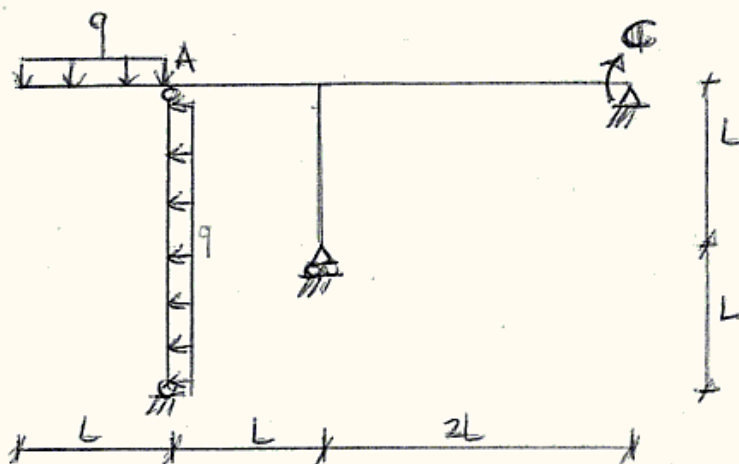
1. Utilizzando il metodo delle forze risolvere la travatura in presenza dei carichi q , C e disegnare i diagrammi delle caratteristiche della sollecitazione (N, T, M).
2. Calcolare la rotazione del nodo A.
3. Risolvere nuovamente la travatura considerando anche un riscaldamento della biella di 20°C e disegnare i nuovi diagrammi delle caratteristiche della sollecitazione (N, T, M) comprensivi sia di q , C che del carico termico.



$$L = 1 \text{ m}, q = 20 \text{ kN/m}, C = 20 \text{ kNm}, P = 20 \text{ kN}$$
$$E = 210 \text{ GPa}, \alpha = 10^{-5} \text{ } ^\circ\text{C}^{-1}$$

La travatura iperstatica di figura è realizzata con profilati IPE 180.

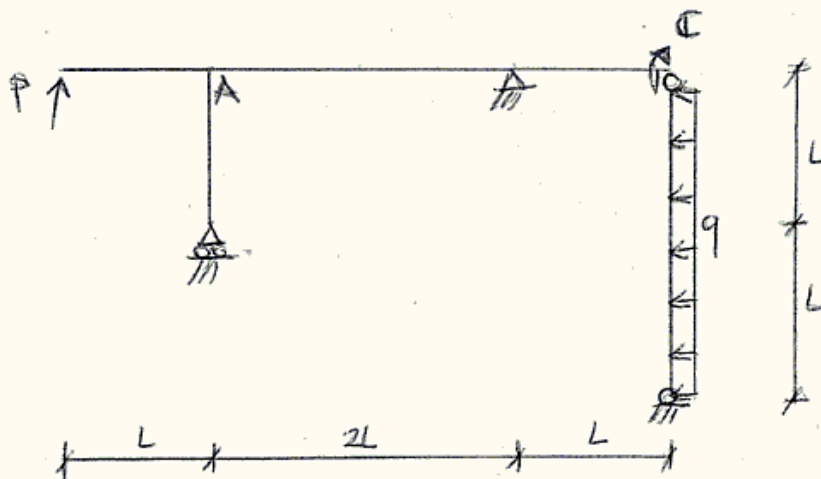
1. Utilizzando il metodo delle forze risolvere la travatura in presenza dei carichi q , C e P e disegnare i diagrammi delle caratteristiche della sollecitazione (N , T , M).
2. Calcolare la rotazione del nodo A .
3. Risolvere nuovamente la travatura considerando anche un riscaldamento della biella di 20°C e disegnare i nuovi diagrammi delle caratteristiche della sollecitazione (N , T , M) comprensivi sia di q , C e P che del carico termico.



$$L = 2 \text{ m}, q = 15 \text{ kN/m}, C = 60 \text{ kNm}$$
$$E = 210 \text{ GPa}, \alpha = 10^{-5} \text{ } ^\circ\text{C}^{-1}$$

La travatura iperstatica di figura è realizzata con profilati IPE 240.

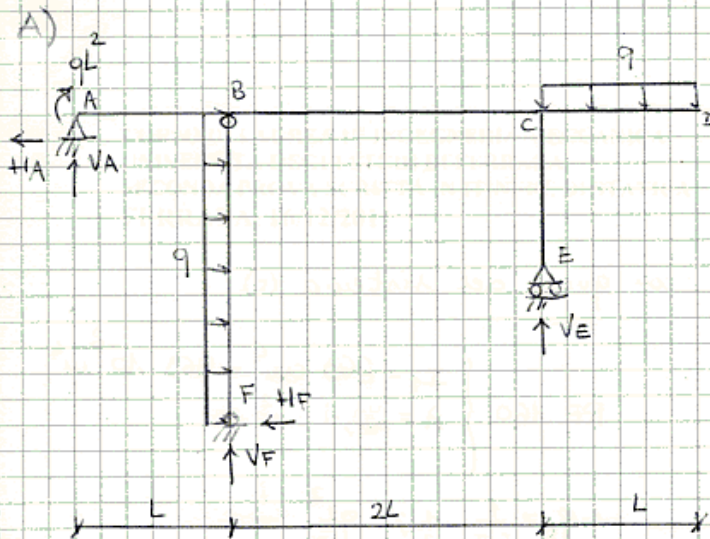
1. Utilizzando il metodo delle forze risolvere la travatura in presenza dei carichi q, C e disegnare i diagrammi delle caratteristiche della sollecitazione (N, T, M).
2. Calcolare la rotazione del nodo A.
3. Risolvere nuovamente la travatura considerando anche un riscaldamento della biella di 20°C e disegnare i nuovi diagrammi delle caratteristiche della sollecitazione (N, T, M) comprensivi sia di q, C che del carico termico.



$$L = 1 \text{ m}, q = 20 \text{ kN/m}, P = 20 \text{ kN}, C = 20 \text{ kNm}$$
$$E = 210 \text{ GPa}, \alpha = 10^{-5} \text{ } ^\circ\text{C}^{-1}$$

La travatura iperstatica di figura è realizzata con profilati IPE 200.

1. Utilizzando il metodo delle forze risolvere la travatura in presenza dei carichi q , C e P e disegnare i diagrammi delle caratteristiche della sollecitazione (N , T , M).
2. Calcolare la rotazione del nodo A .
3. Risolvere nuovamente la travatura considerando anche un riscaldamento della biella di 20°C e disegnare i nuovi diagrammi delle caratteristiche della sollecitazione (N , T , M) comprensivi sia di q , C e P che del carico termico.



$$(B \uparrow)_{BF} \quad H_F = qL = \frac{1}{2} qL^2$$

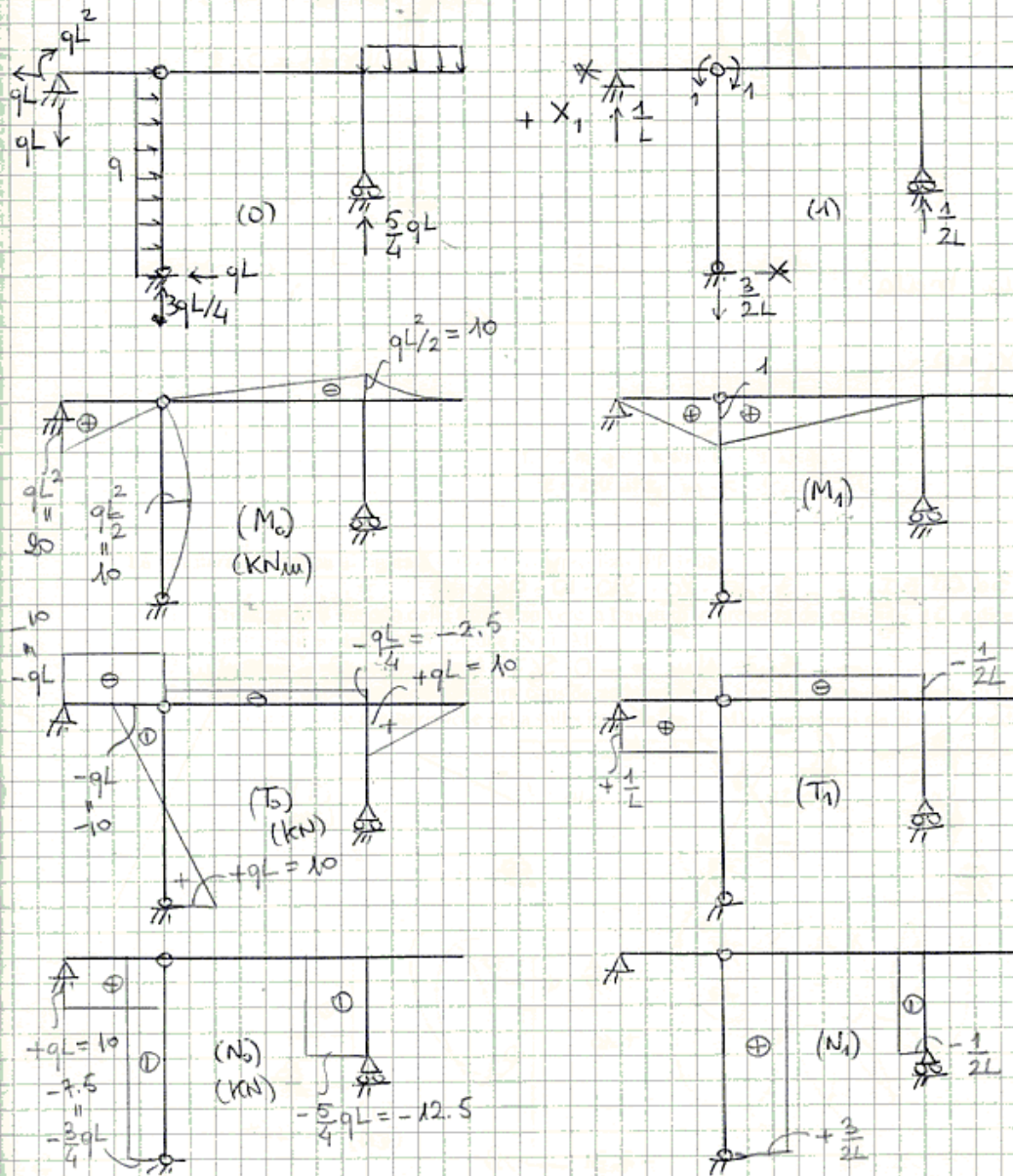
$$(\leftarrow) \quad H_A = 2qL - H_F = qL$$

$$(\uparrow) \quad V_A + V_F + V_E = qL$$

$$(B \uparrow) \quad V_A L + qL^2 = V_E 2L - qL \frac{5}{2} L$$

Trudatwa 1 voica ipostatice.

Jucoguta ipostatice: $X_1 = M_B$



$$EI_1 \eta_{10} = \frac{1}{6} q L^2 \cdot L - \frac{1}{6} q \frac{L^2}{2} \cdot 2L = 0$$

$$EI_1 \eta_{11} = \frac{1}{3} L + \frac{1}{3} 2L = L$$

$$X_1 = - \frac{\eta_{10}}{\eta_{11}} = 0$$

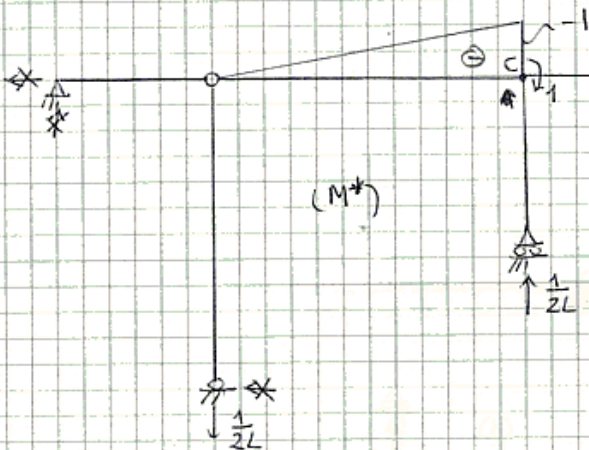
I diagrammi delle .e.s. coincidono con quelli del sistema (0).

Rotazione in C:

$$\text{IPE 160} \left\{ \begin{array}{l} I_1 = 863 \text{ cm}^4 = 863 \cdot 10^{-8} \text{ m}^4 \\ A = 20,1 \text{ cm}^2 \end{array} \right.$$

$$1 \cdot \varphi_c = \frac{1}{EI_1} \frac{1}{3} 2L \frac{qL^2}{2}$$

$$\varphi_c = \frac{qL^3}{3EI_1} = \frac{5 \cdot 10^3 \cdot 8}{210 \cdot 10^9 \cdot 3 \cdot 863 \cdot 10^{-8}} = 0,0073 = 0,42^\circ$$

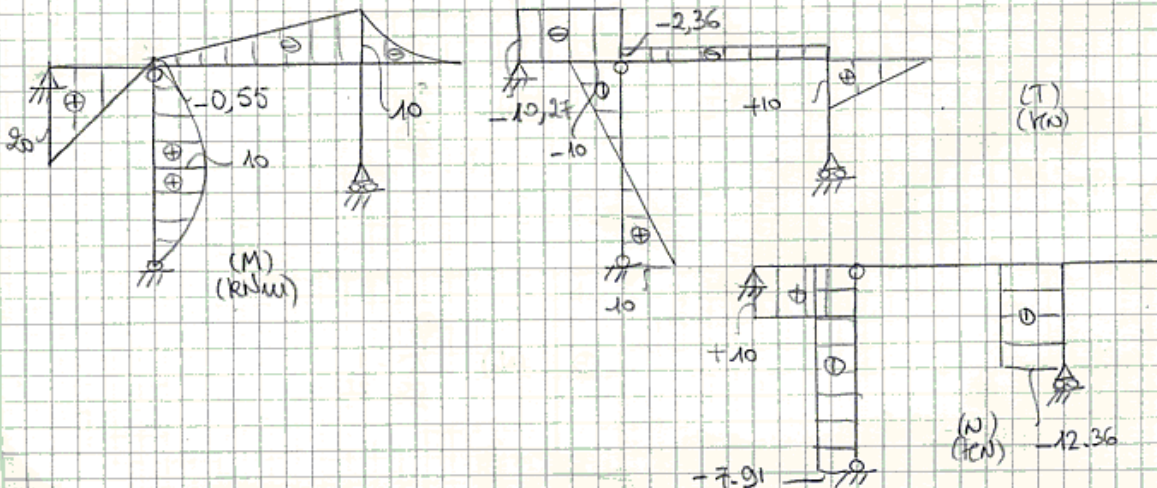


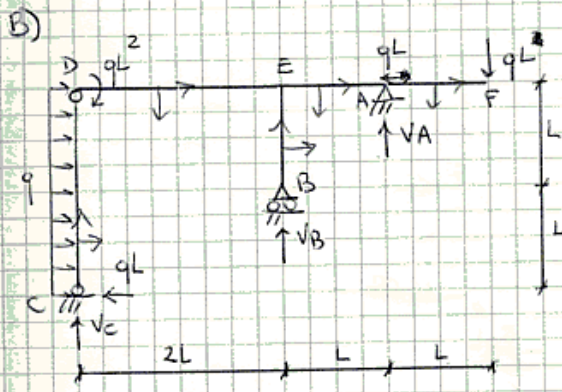
Riscalcolamento della biella.

$$\eta_{11c} + \eta_{110} + \eta_{11} X_1 = 0$$

$$\eta_{11c} = \frac{3 \alpha \Delta T \cdot 2L}{2L}$$

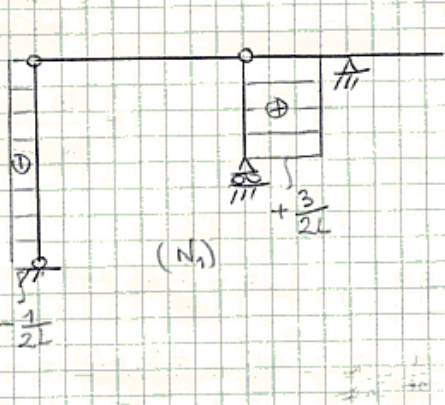
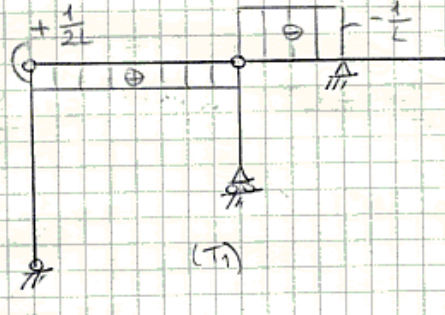
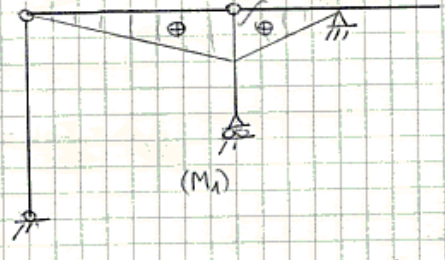
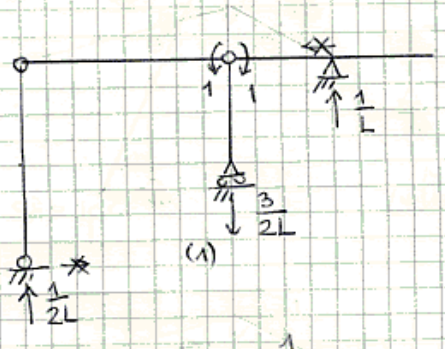
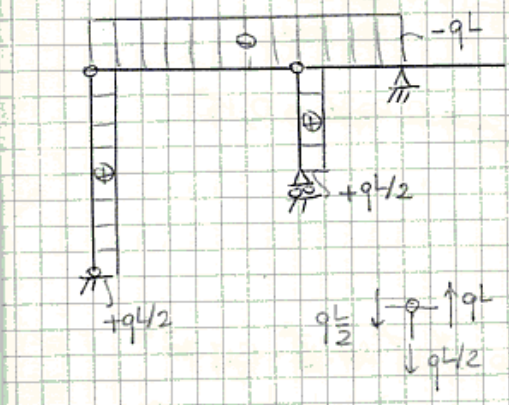
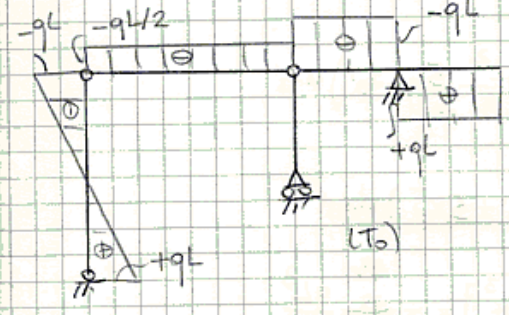
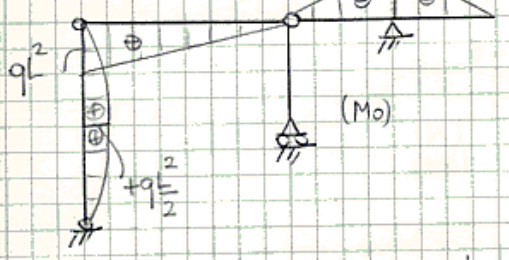
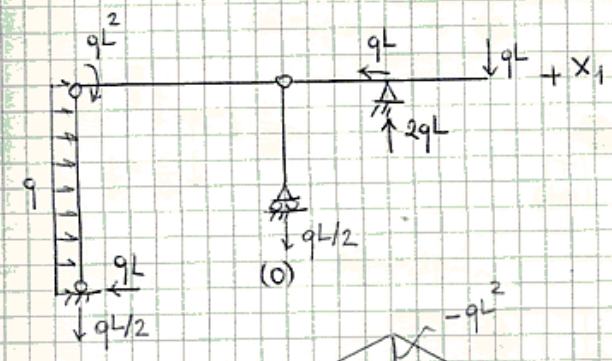
$$X_1 = - \frac{\eta_{11c}}{\eta_{11}} = - \frac{3 \alpha \Delta T EI_1}{L} = - \frac{3 \cdot 10^{-5} \cdot 20 \cdot 210 \cdot 10^9 \cdot 863 \cdot 10^{-8}}{2} = -547 \text{ Nm} = -0,547 \text{ kNm} \approx -0,55 \text{ kNm}$$





$$\begin{cases} V_A 3L + V_B 2L = qL^2 + 4qL^2 \\ V_A + V_B + V_C = qL \end{cases}$$

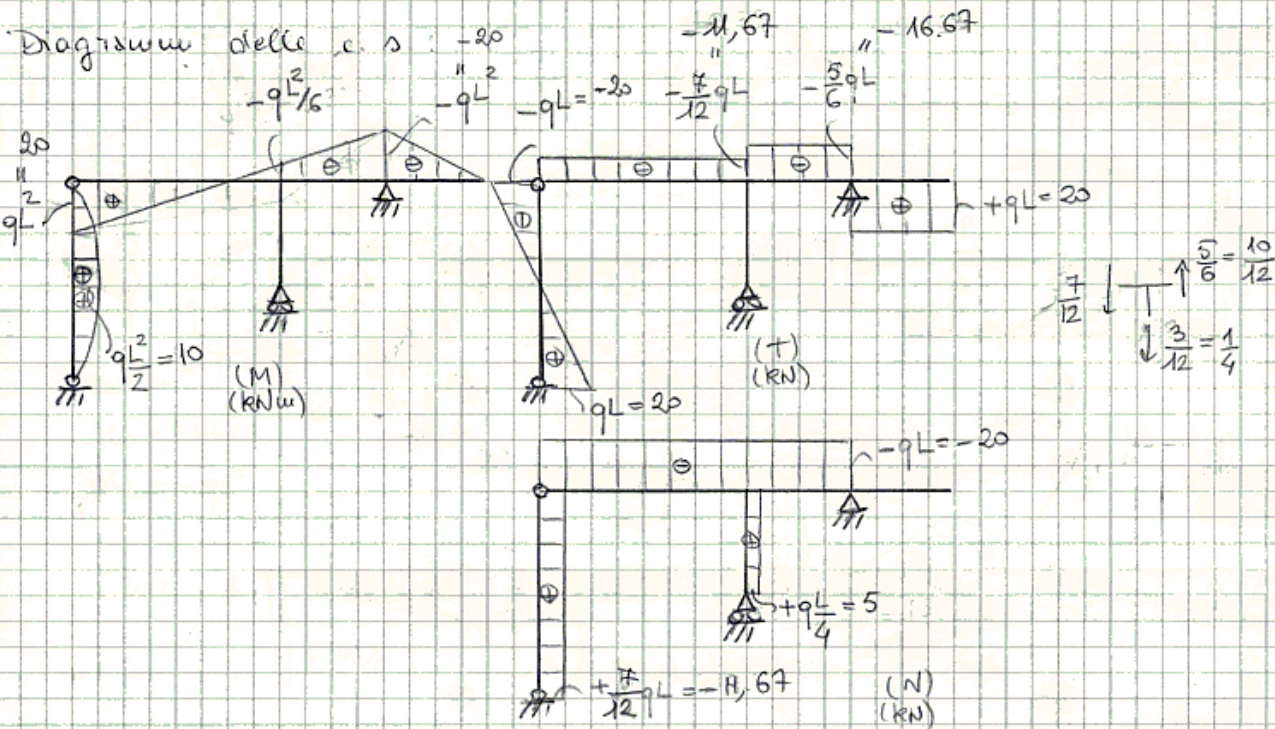
Trabattina me weta iperstatica
 Jucogweta iperstatica: $X_1 = ME$



$$EI_1 \eta_{10} = + \frac{1}{6} 2L q L^2 + \frac{1}{6} q L^3 = + \frac{q L^3}{6}$$

$$EI_1 \eta_{11} = \frac{1}{3} 2L + \frac{1}{3} L = L$$

$$X_1 = - \frac{\eta_{10}}{\eta_{11}} = - \frac{q L^2}{6} = -3.33 \text{ kNm}$$



Rotazione in A:

$$1 \cdot \psi_A = \frac{1}{EI_1} \int_0^L \left(-\frac{x_3'}{L} \right) \left(\frac{qL^2}{6} - \frac{5}{6} qL x_3' \right) dx_3'$$

$$= + \frac{1}{EI_1} \frac{qL^3}{6} \int_0^L (L x_3' + 5 x_3'^2) dx_3'$$

$$= + \frac{qL^3}{6EI_1} \left[\frac{L}{2} + \frac{5L^3}{3} \right] = + \frac{13}{36} \frac{qL^3}{EI_1}$$

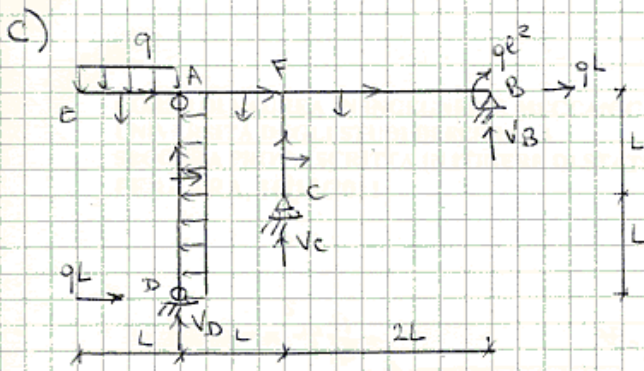
$$= \frac{13 \cdot 20 \cdot 10^3}{36 \cdot 210 \cdot 10^8 \cdot 1317 \cdot 10^8} = 0,0026 = 0,15^\circ$$

Carico termico:

$$\eta_{1e} + \eta_{10} + \eta_{11} X_1 = 0, \quad \eta_{1e} = - \frac{1}{2L} 2L \alpha \Delta T = -\alpha \Delta T$$

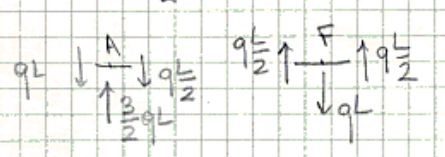
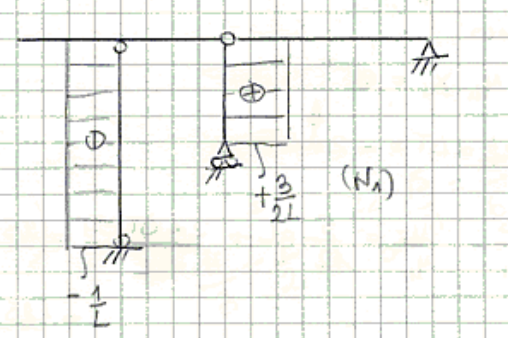
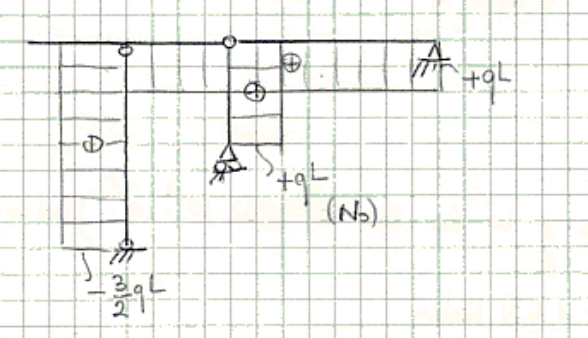
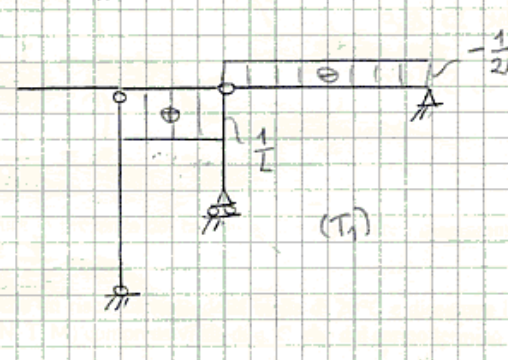
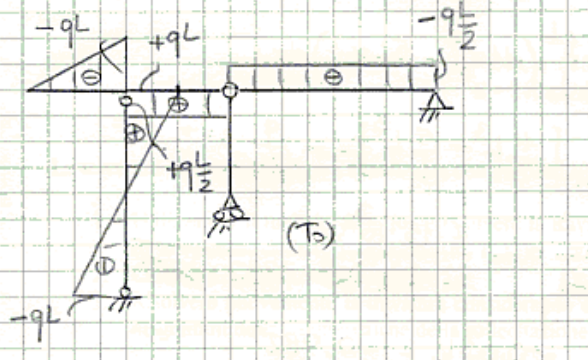
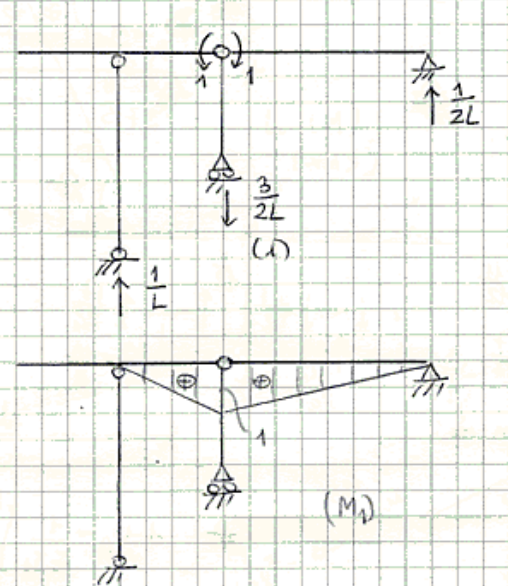
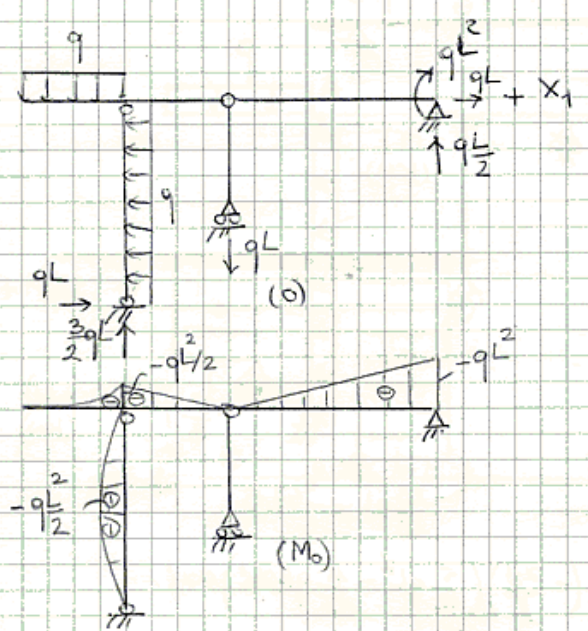
$$X_1 = - \frac{\eta_{10}}{\eta_{11}} - \frac{\eta_{1e}}{\eta_{11}} = - \frac{qL^2}{6} + \frac{EI_1 \alpha \Delta T}{L} = -3.33 + \frac{210 \cdot 10^8 \cdot 20 \cdot 10^{-8} \cdot 1317 \cdot 10^{-8}}{1317 \cdot 10^8} = (-3.33 + 0,55) \text{ kNm} = -2,77 \text{ kNm}$$

Occorre rifare i diagrammi.



$$\begin{cases} V_B 2L - qL^2 + 2qL^2 - V_D L - 2qL^2 + 2qL^2 = 0 \\ V_B + V_C + V_D = qL \end{cases}$$

Struttura una volta iperstatica
 Incognita iperstatica: $X_1 = M_F$

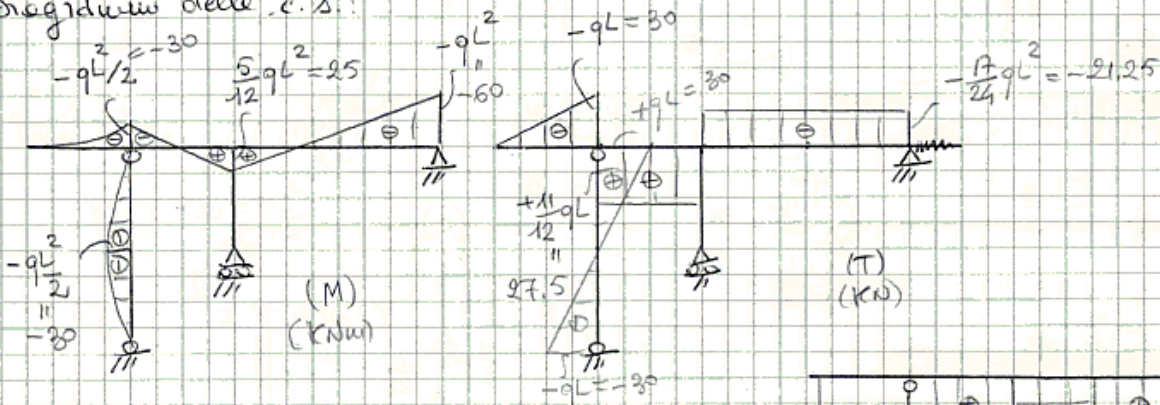


$$EI_1 \eta_{10} = -\frac{1}{6} L q \frac{L^2}{2} - \frac{1}{6} 2L q L^2 = -\frac{5}{12} q L^3$$

$$EI_1 \eta_{11} = \frac{L}{3} + \frac{2}{3} L = L$$

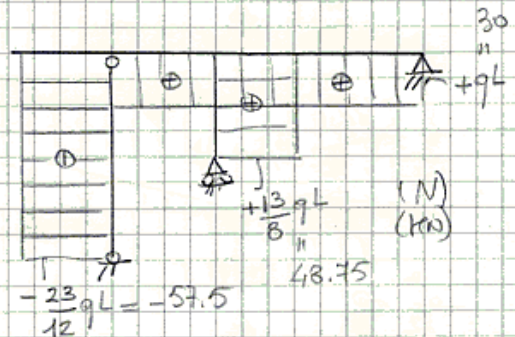
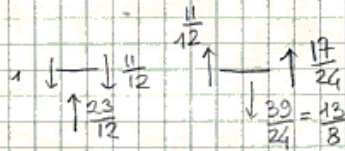
$$X_1 = -\frac{\eta_{10}}{\eta_{11}} = \frac{5}{12} q L^2 = 25 \text{ kNm}$$

Diagrammi delle c.s.:

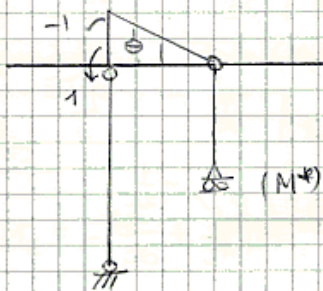


$$\frac{5}{12} + \frac{6}{2 \cdot 6} = \frac{11}{12}$$

$$\frac{5}{12} + 1 = \frac{17}{12}$$



Rotazione w_A :



$$1 \cdot \varphi_A = \frac{1}{EI_1} \int_0^L \left(-\frac{x_3'}{L} \right) \left(\frac{5}{12} q L^2 - \frac{11}{12} q L x_3' \right) dx_3'$$

$$= -\frac{q}{12EI_1} \int_0^L (11x_3'^2 - 5Lx_3') dx_3'$$

$$= -\frac{q}{12EI_1} \left[\frac{11}{3} L^3 - \frac{5}{2} L^3 \right] = -\frac{q}{12EI_1} \cdot \frac{7}{6} L^3$$

$$= -\frac{7}{72} \frac{q L^3}{EI_1} = -\frac{7 \cdot 15 \cdot 10^3 \cdot 8}{72 \cdot 210 \cdot 10^8 \cdot 3892 \cdot 10^{-8}}$$

$$= -0,0016 = -0,082^\circ$$

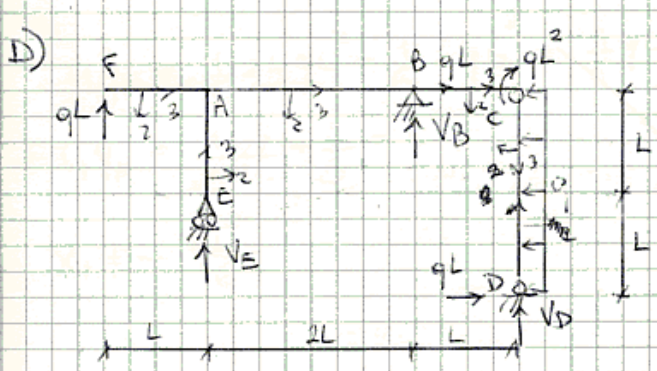
Carico termico:

$$M_{1t} + \eta_{10} + \eta_{11} X_1 = 0$$

$$\eta_{1t} = -\frac{1}{L} 2L \alpha \Delta T = -2\alpha \Delta T$$

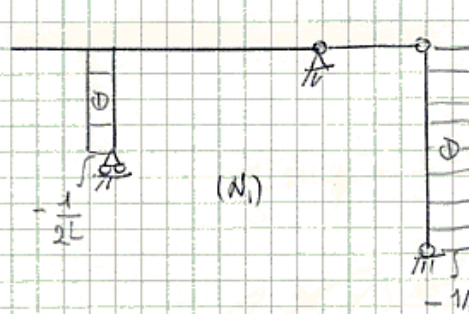
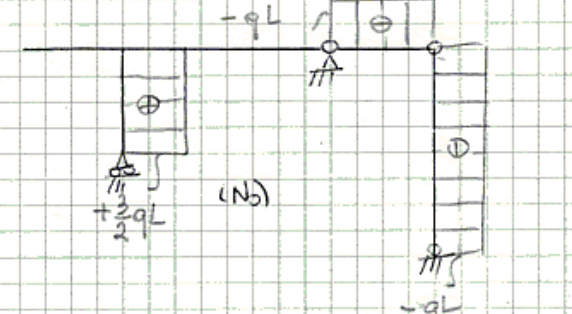
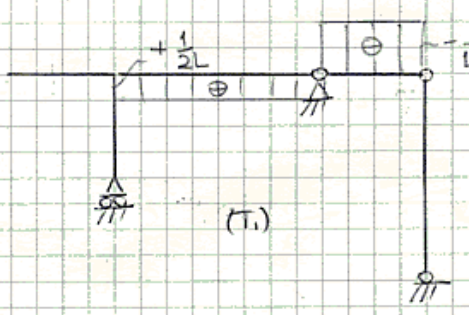
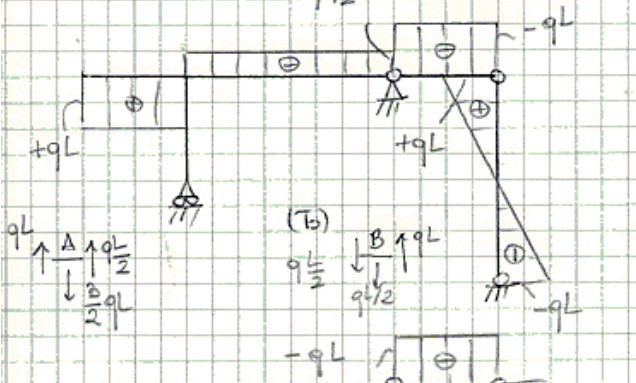
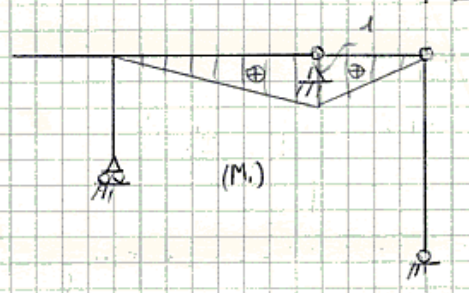
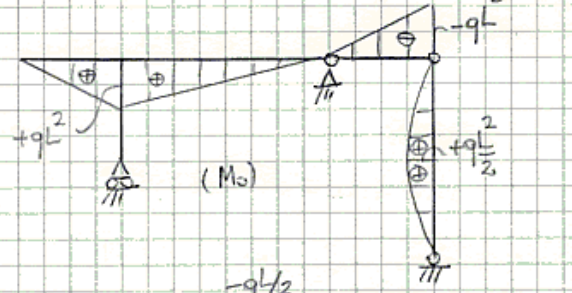
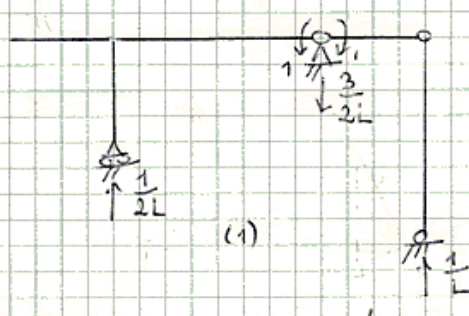
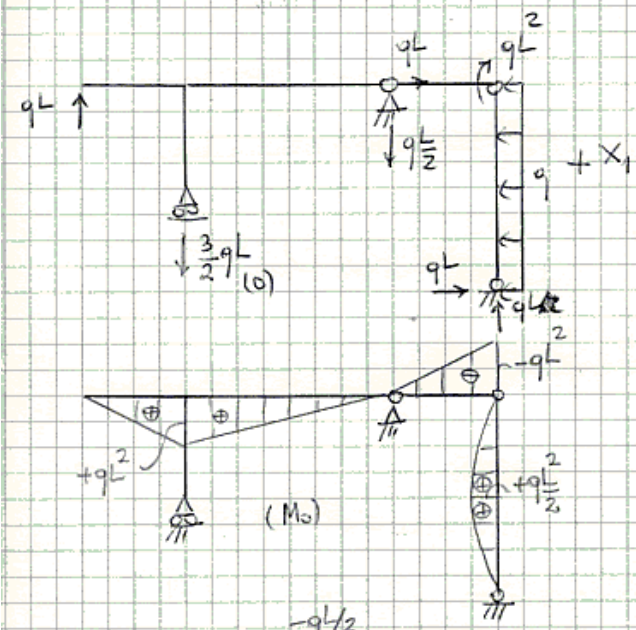
$$X_1 = -\frac{\eta_{10}}{\eta_{11}} - \frac{\eta_{1t}}{\eta_{11}} = \frac{5}{12} q L^2 + \frac{2\alpha \Delta T EI_1}{L} = \left(25 + \frac{2 \cdot 10^{-5} \cdot 20 \cdot 210 \cdot 10^9 \cdot 3892 \cdot 10^{-8} \cdot 10^{-3}}{7} \right) \text{ kNm}$$

$$= (25 + 1,63) \text{ kNm}$$



$$\begin{cases} V_B 2L + V_D 3L - qL^2 - qL^2 + 2qL^2 - qL^2 = 0 \\ V_E + V_B + V_D = -qL \end{cases}$$

Travatura ucid vortu iperstatico
 Discegnatu iperstatico $X_1 = M_B$

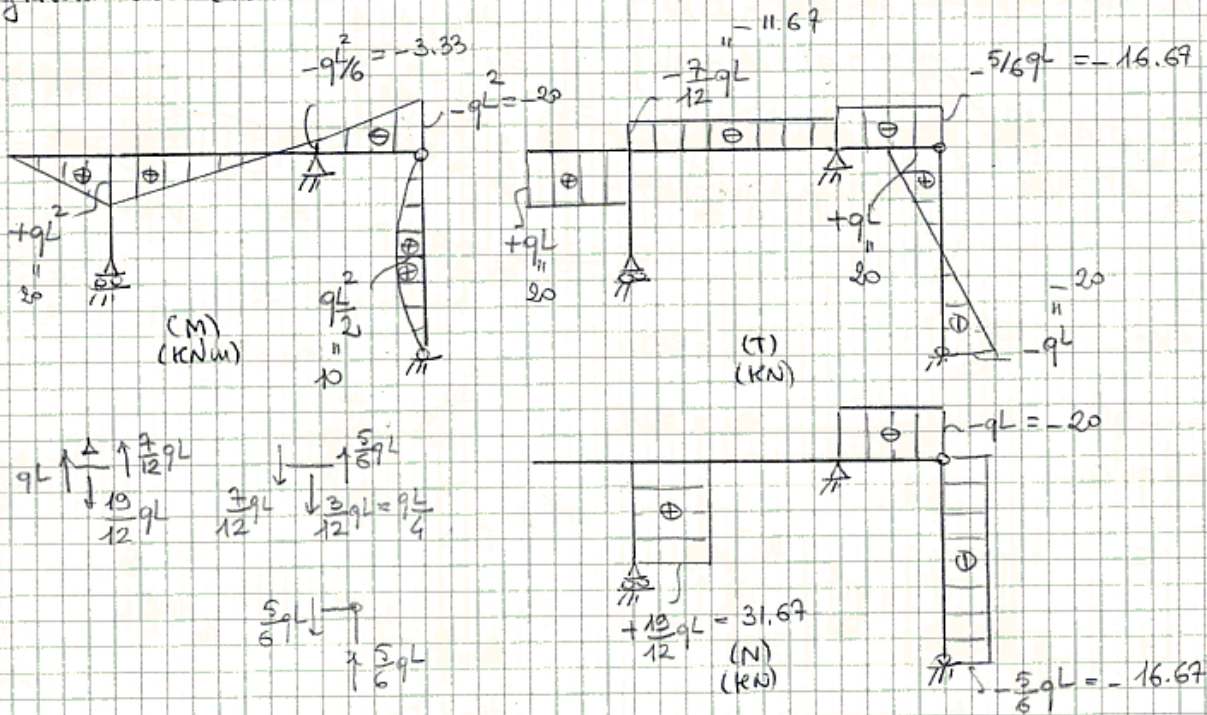


$$EI_1 y_{10} = \frac{1}{6} 2L qL^2 - \frac{1}{6} L qL^2 = \frac{1}{6} qL^3$$

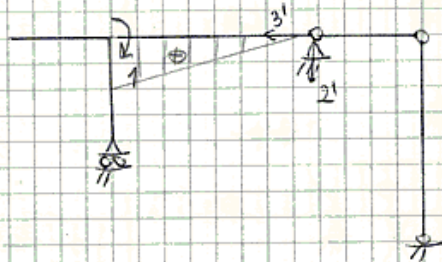
$$EI_1 y_{11} = \frac{1}{3} 2L + \frac{L}{3} = L$$

$$X_1 = -y_{10}/y_{11} = -qL/6 = -3.33 \text{ KNW}$$

Diagrammi delle c.s.:



Rotazione w_A :



$$\begin{aligned}
 1. \varphi_A &= \frac{1}{EI} \int_0^{2L} \left(\frac{x_3'}{2L} \right) \left(-q \frac{x_3'}{2} + \frac{7}{12} q L x_3' \right) dx_3' \\
 &= \frac{q}{24EI} \int_0^{2L} \left(-2L x_3' + 7 x_3'^2 \right) dx_3' \\
 &= \frac{q}{24EI} \left[-2L \frac{x_3'^2}{2} + \frac{7}{3} x_3'^3 \right]_0^{2L} = \frac{44}{3} \frac{qL^3}{24EI} = \frac{11}{18} \frac{qL^3}{EI} \\
 &= \frac{11 \cdot 20 \cdot 10^3}{18 \cdot 210 \cdot 10^9 \cdot 1943 \cdot 10^{-8}} = 0,003 = 0,17^\circ
 \end{aligned}$$

Carico termico:

$$M_{1t} + M_{10} + M_{11} X_1 = 0$$

$$M_{1t} = -\frac{1}{L} \alpha \Delta T 2L = -2 \alpha \Delta T$$

$$\begin{aligned}
 X_1 &= -\frac{qL^2}{6} + \frac{EI 2 \alpha \Delta T}{L} = \left(-3.33 + \frac{210 \cdot 10^9 \cdot 1943 \cdot 10^{-8} \cdot 2 \cdot 10^{-5} \cdot 20}{1} \cdot 10^{-3} \right) \text{ kNm} \\
 &= (-3.33 + 1.63) \text{ kNm} = -1.7 \text{ kNm}
 \end{aligned}$$

Oltre a che i diagrammi.