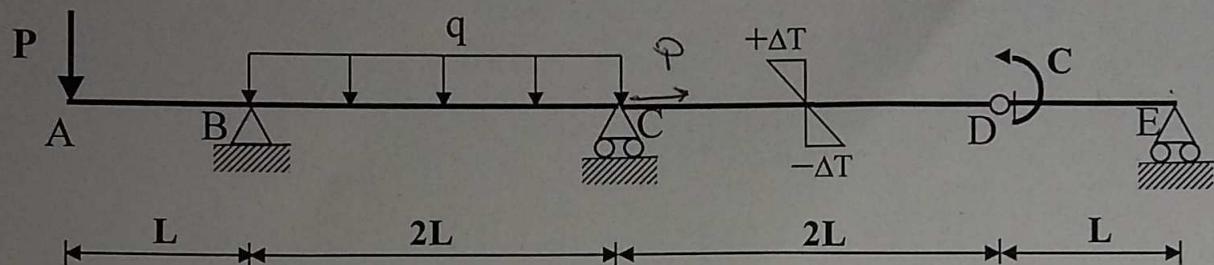


CORSO DI LAUREA IN INGEGNERIA MECCANICA
 UNIVERSITÀ DI FERRARA
 PROVA SCRITTA DI STATICÀ
 01/06/2016

A



$$L = 1 \text{ m}, q = 20 \text{ kN/m}, P = 20 \text{ kN}, C = 40 \text{ kNm}, \\ E = 210 \text{ GPa}, \sigma_{\text{amm}} = 240 \text{ MPa}, \Delta T = +10^\circ \text{C}, \alpha = 10^{-5} \text{ }^\circ\text{C}^{-1}$$

La travatura isostatica in figura deve essere realizzata con profilati IPE.

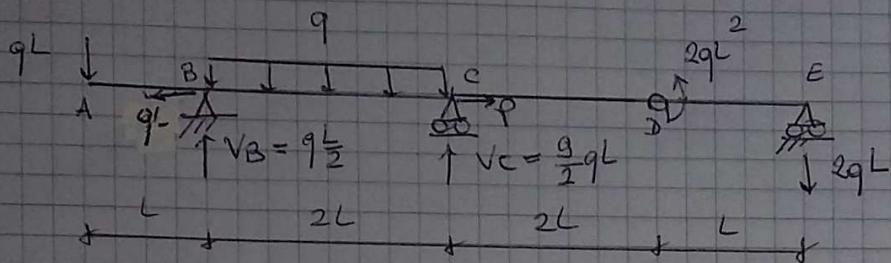
- Disegnare i diagrammi quotati delle caratteristiche della sollecitazione.
- Dimensionare la travatura.
- Calcolare la rotazione relativa nella cerniera in D.
- Calcolare la rotazione relativa in D considerando in aggiunta al carico anche la presenza di un carico termico a farfalla ΔT sul tratto CDE.

SOLUZIONE FILA A.

$$qL = 20 \text{ RN} = P$$

$$qL^2 = 20 \text{ RN m}$$

$$\Gamma = 2qL^2$$



$$\begin{cases} V_B + V_C = qL + 2qL + 2qL = 5qL \\ V_B qL + V_C 2L - 5qL^2 - 2qL 3L = 0 \end{cases}$$

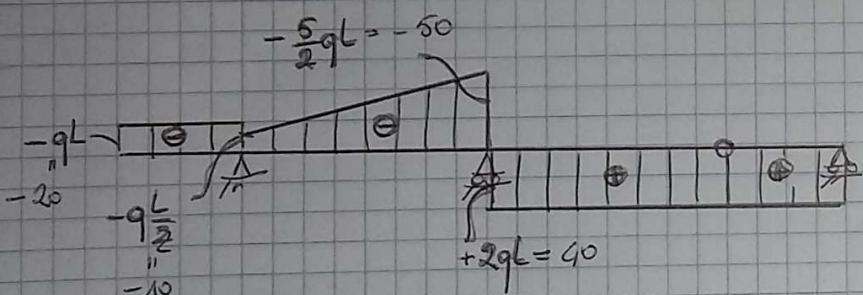
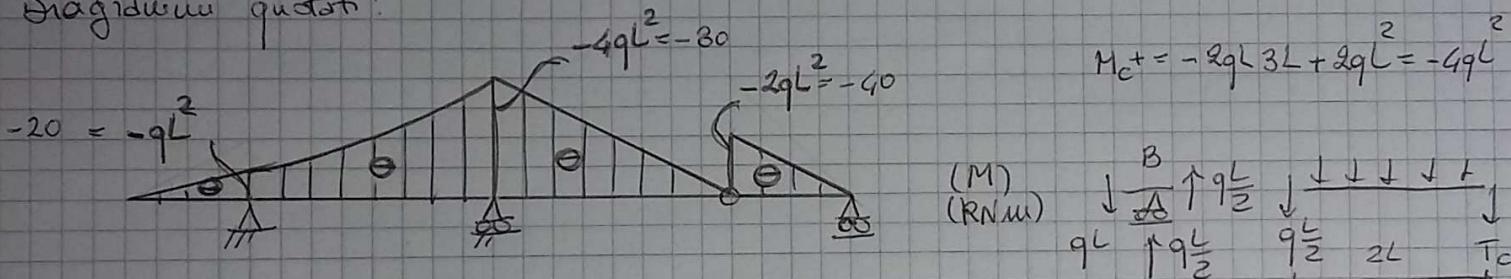
$$\begin{cases} V_B + V_C = 5qL & (\times -2) \\ 4V_B + 2V_C = 11qL \end{cases}$$

$$\begin{cases} V_B = qL/2 \\ V_C = 5qL - V_B = 5qL - qL/2 = \frac{9}{2}qL \end{cases}$$

$$4V_B - 2V_B + 2V_C - 2V_C = 11qL - 10qL$$

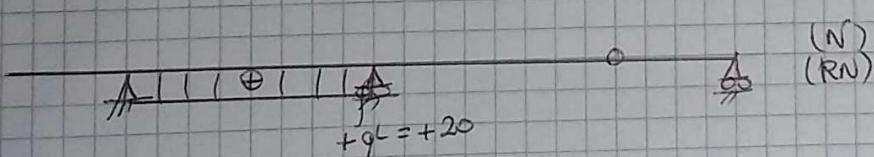
$$2V_B = qL$$

Diagramma di quantità:



$$(T)_{(RN)} \quad \frac{qL}{2} \downarrow \frac{2qL}{\Delta} \downarrow \frac{qL}{2} \downarrow \frac{qL}{2} \downarrow 2L \downarrow T_C$$

$$T_C = -qL/2 - 2qL = -\frac{5}{2}qL$$



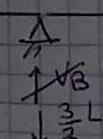
Dimensionamento:

$$W_1 \geq \frac{qL^2}{G \cdot A} = \frac{20 \cdot 10^3}{290 \cdot 10^6} \text{ m}^3 = 333 \text{ cm}^3$$

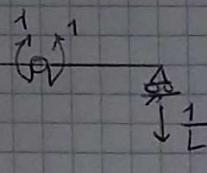
$$\rightarrow \text{IPE } 270 \quad \begin{cases} W_1 = 428,9 \text{ cm}^3 \\ I_1 = 5790 \text{ cm}^4 \\ H = 27 \text{ cm} \\ A = 15,95 \text{ cm}^2 \end{cases}$$

A

Rotazione relativa w D:



$$\uparrow v_C = \frac{5}{2}L$$



$$\begin{cases} V_B + V_C = \frac{1}{L} \\ V_B 4L + V_C 2L + 1 = 0 \end{cases}$$

$$\begin{cases} V_B + V_C = 1/L \\ 4V_B + 2V_C = -1/L \end{cases}$$

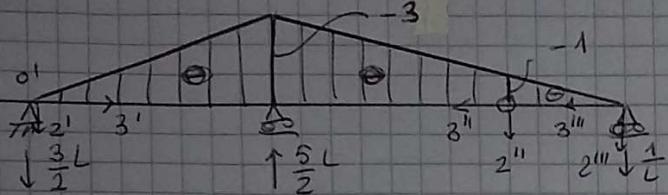
$\times (-2)$

$$4V_B - 2V_B + 2V_C - 2V_C = -\frac{1}{L} - \frac{2}{L}$$

$$2V_B = -\frac{3}{L}$$

$$V_B = -\frac{3}{2L}$$

$$V_C = \frac{1}{2L} + \frac{3}{2}L = \frac{5}{2}L$$



(M*)

$$1. \Delta \varphi_D^1 = \frac{1}{EI_1} \int_0^{2L} \left(-q \frac{x_3'^2}{2} - q \frac{L}{2} x_3' - qL^2 \right) \left(-\frac{3}{2L} x_3' \right) dx_3' + \frac{1}{EI_1} \int_0^{2L} \left(-1 - \frac{x_3''}{L} \right) \left(-2qL x_3'' \right) dx_3''$$

$$+ \frac{1}{EI_1} \int_0^{2L} \left(-2qL x_3''' \right) \left(-\frac{x_3'''}{L} \right) dx_3'''$$

$$= \frac{1}{EI_1} \left(8qL^3 + \frac{28}{3}qL^3 + \frac{2}{3}qL^3 \right) = \frac{18qL^3}{EI_1} = \frac{18 \cdot 20 \cdot 10^3}{210 \cdot 108 \cdot 5790 \cdot 10^8} = 0,0296$$

1,7°

Carico termico:

$$1. \Delta \varphi_D^{\Delta T} = \int_{CDE} M^* x_t dx_3 = x_t \int_{CDE} M^* dx_3 = \left(-\frac{\alpha \Delta T}{H} \right) \left(-3L \cdot \frac{3}{2} \right) = \frac{9 \alpha \Delta T L}{H}$$

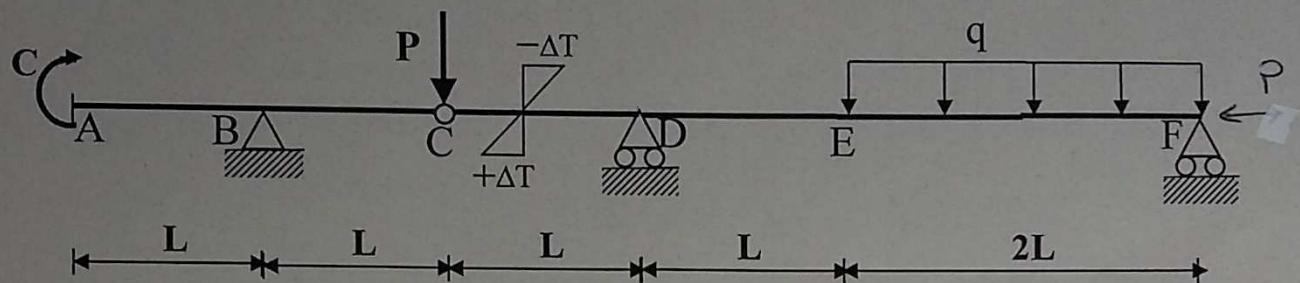
$$= \frac{9 \cdot 10^{-8} \cdot 10}{0,27} = 0,0033$$

$$= 0,13^\circ$$

$$\Delta \varphi_D^{\text{TOT}} = \frac{9 \alpha \Delta T L}{H} + \frac{18qL^3}{EI_1} = 1,89^\circ$$

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B



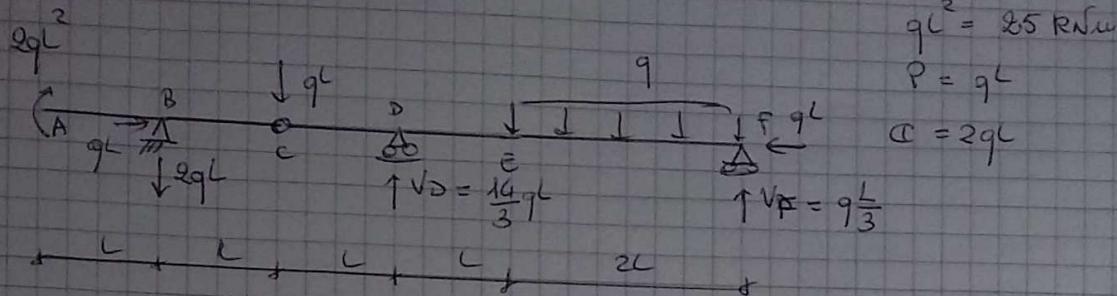
$$L = 1 \text{ m}, q = 25 \text{ kN/m}, P = 25 \text{ kN}, C = 50 \text{ kNm}, \\ E = 210 \text{ GPa}, \sigma_{amm} = 240 \text{ MPa}, \Delta T = +10^\circ \text{C}, \alpha = 10^{-5} \text{ }^\circ\text{C}^{-1}$$

La travatura isostatica in figura deve essere realizzata con profilati IPE.

- Disegnare i diagrammi quotati delle caratteristiche della sollecitazione.
- Dimensionare la travatura.
- Calcolare la rotazione relativa nella cerniera in C.
- Calcolare la rotazione relativa in C considerando in aggiunta al carico anche la presenza di un carico termico a farfalla ΔT sul tratto ABCD.

6

SOLUTIONE FILA B



$$qL = 25 \text{ kN}$$

$$qL^2 = 25 \text{ kNm}$$

$$P = qL$$

$$A = 2qL$$

$$\begin{cases} V_D + V_F = 2qL + qL + 2qL = 5qL \\ V_D + V_F = 2qL \end{cases}$$

$$\begin{cases} V_D + V_F = 5qL & (\times (-1)) \\ V_D + 4V_F = 6qL \end{cases}$$

$$3V_F = qL$$

$$V_D = 5qL - V_F$$

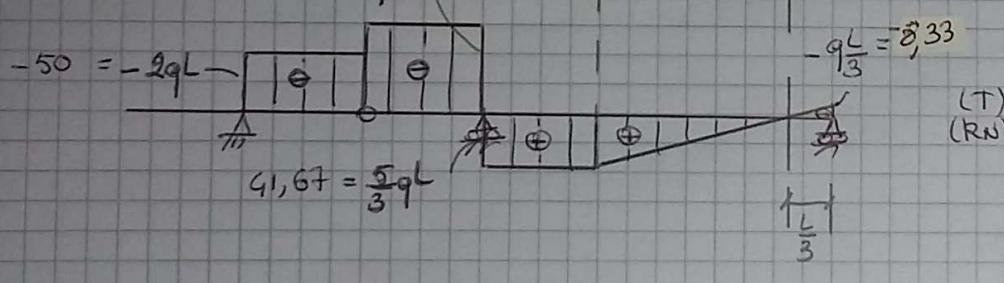
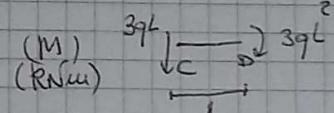
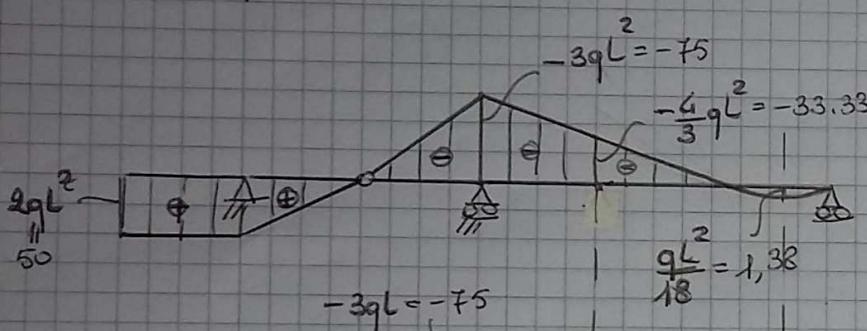
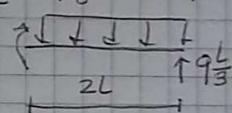
$$V_F = qL/3$$

$$V_D = \frac{14}{3}qL$$

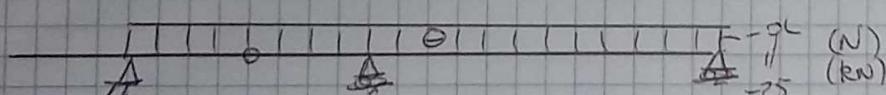
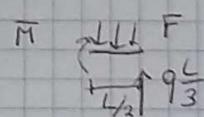
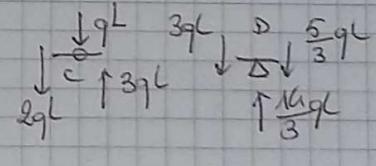
$$V_D + 4V_F - V_D - V_F = 6qL - 5qL = qL$$

Diagramma dei momenti:

$$M_E = \frac{qL}{3} zL - 2qL^2 = -\frac{4}{3}qL^2$$



$$(T) (RN)$$



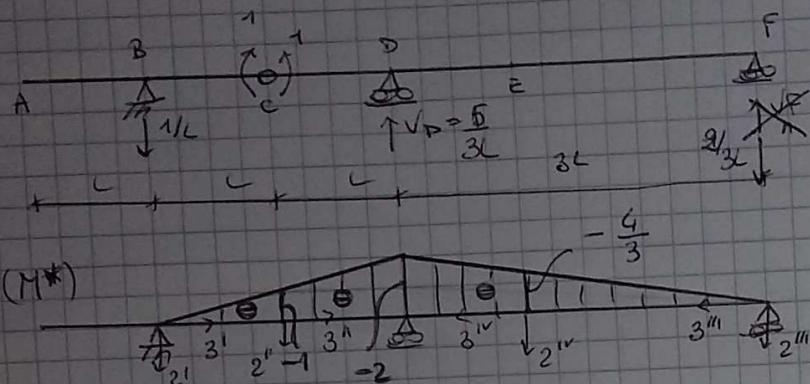
$$M = qL \frac{L}{3} - \frac{1}{2} qL \frac{L}{3} = \frac{qL^2}{18}$$

Dimensionamento:

$$W_1 \geq \frac{3qL^2}{64M} = \frac{75 \cdot 10^3 \cdot 10^6}{240 \cdot 10^6} \text{ cm}^3 = 312,5 \text{ cm}^3 \rightarrow \text{IPE } 290$$

$$\begin{cases} W_1 = 324,3 \text{ cm}^3 \\ I_1 = 3892 \text{ cm}^4 \\ H = 24 \text{ cm} \\ A = 39,12 \text{ cm}^2 \end{cases}$$

stabilità relativa in C:



$$\begin{cases} V_D + V_F = 1/L & (x(-L)) \\ V_DL + V_F GL + 1 = 0 \end{cases}$$

$$V_DL + V_F GL - V_DL - V_F L + 1 = -1$$

$$3VFL = -8$$

$$V_F = -8/3L$$

$$V_D = 1/L + \frac{2}{3L} = \frac{5}{3L}$$

$$1. \Delta \varphi_C^q = \frac{1}{EI_1} \int_0^L (2qL^2 - 2qLx_3') \left(-\frac{1}{L}x_3' \right) dx_3' + \frac{1}{EI_1} \int_0^L (-3q(x_3'')) \left(-1 - \frac{x_3''}{L} \right) dx_3''$$

$$+ \frac{1}{EI_1} \int_0^{2L} \left(-q \frac{x_3'''^2}{2} + q \frac{L}{3} x_3''' \right) \left(-\frac{2}{3L} x_3''' \right) dx_3''' + \frac{1}{EI_1} \int_0^L \left(-\frac{4}{3}qL^2 - \frac{5}{3}qLx_3'' \right) \left(-\frac{4}{3} - \frac{2}{3L} x_3'' \right) dx_3''$$

$$= \frac{1}{EI_1} \left[-q \frac{L^3}{3} + \frac{5}{2}qL^3 + \frac{20}{27}qL^3 + \frac{100}{27}qL^3 \right] = \frac{119}{18} \frac{qL^3}{EI_1} = \frac{119 \cdot 25 \cdot 10}{18 \cdot 210 \cdot 18} \frac{32}{3892} \cancel{N^2}$$

$$1,02 = 1,16^\circ$$

Carcico termico:

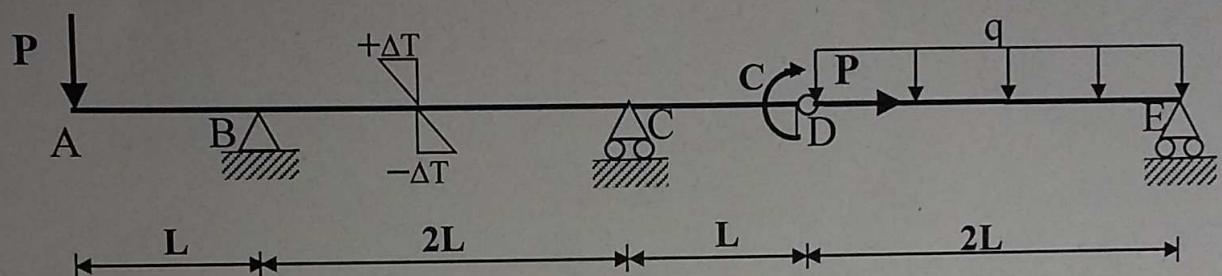
$$1. \Delta \varphi_C^{\Delta T} = \int_{ABCD} x_t H^* dx_3' = x_t \cdot \int_{ABCD} H^* dx_3' = \frac{2x \Delta T}{H} \left(-\frac{2L \cdot L}{2} \right)$$

$$= -\frac{4x \Delta T L}{H} = -\frac{4 \cdot 10^{-8} \cdot 18}{0,24} = -0,0016 = -0,095^\circ$$

$$\Delta \varphi_C^{\text{TOT}} = \Delta \varphi_C^q + \Delta \varphi_C^{\Delta T} = 1,16^\circ - 0,095^\circ = 1,065^\circ$$

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C

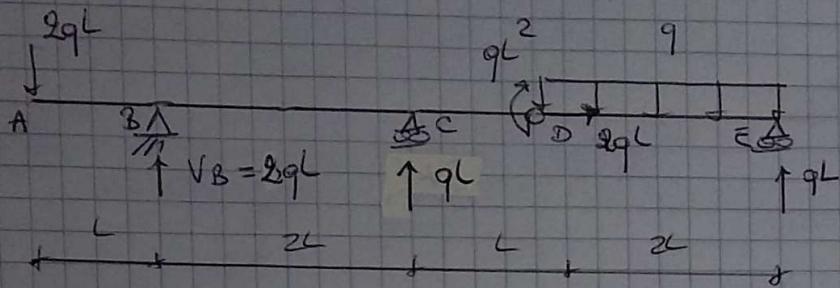


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DWYONE FILAC



$$qL = 20 \text{ kN}$$

$$qL^2 = 20 \text{ kN}$$

$$P = 2qL$$

$$C = qL^2$$

$$\left\{ V_B + V_C = 2qL + 2qL - qL = 3qL \right.$$

$$\left\{ V_B 34 + V_C 24 + qL^2 - 2qL 4K = 0 \right.$$

$$\left\{ V_B + V_C = 3qL \quad (\times (-1)) \right.$$

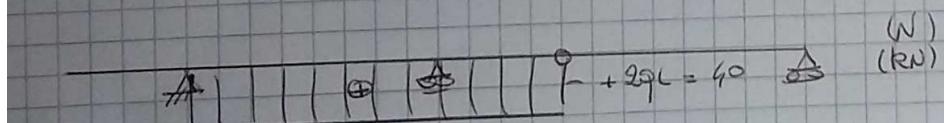
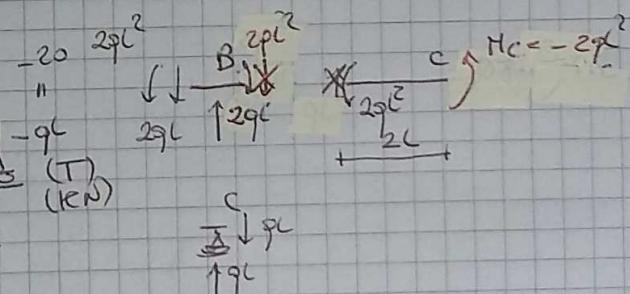
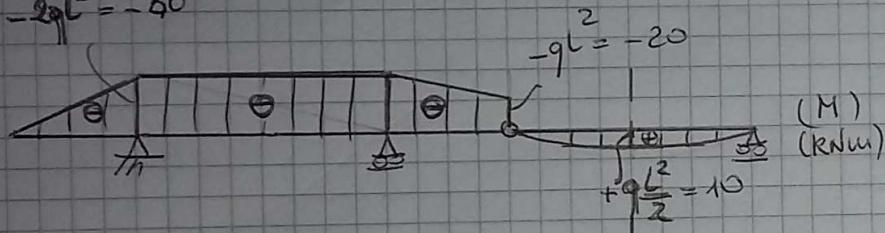
$$\left\{ 3V_B + V_C = 7qL \right.$$

$$\left\{ \begin{array}{l} V_B = 2qL \\ V_C = qL \end{array} \right.$$

$$3V_B + V_C - 2V_B - V_C = (7 - 3)qL = 4qL$$

Diagrammi quozienti:

$$-2qL^2 = -40$$

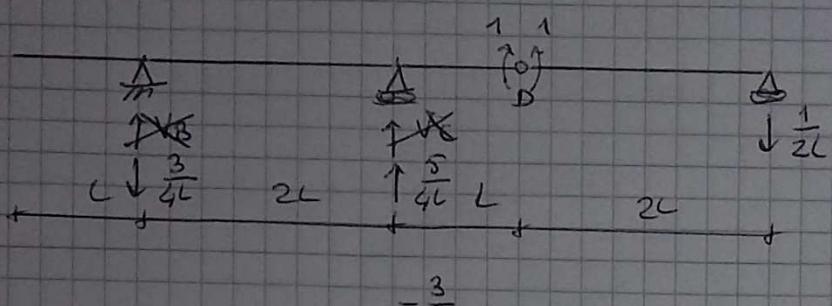


Dimensionamenti:

$$W_1 > \frac{2qL^2}{64Mn} = \frac{2q \cdot 10^3 \cdot 10^6}{64 \cdot 0.12 \cdot 10^6} \text{ cm}^3 = 167 \text{ cm}^3 \rightarrow \text{IPE } 200$$

$$\left\{ \begin{array}{l} W_1 = 194.3 \text{ cm}^3 \\ I_1 = 1943 \text{ cm}^4 \\ H = 20 \text{ cm} \\ A = 26.48 \text{ cm}^2 \end{array} \right.$$

Rotationsrelativa in D:



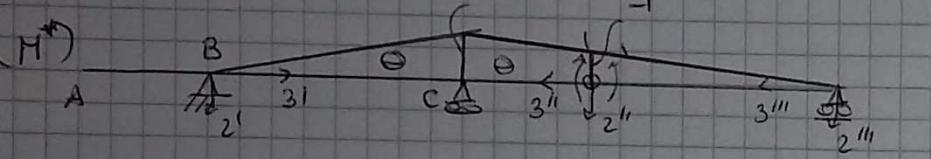
$$\begin{cases} V_B 3L + V_C L + 1 = 0 \\ V_B + V_C = \frac{1}{2L} \end{cases}$$

$$\begin{cases} V_B + V_C = \frac{1}{2L} & (\times (-1)) \\ 3V_B + V_C = -\frac{1}{L} \end{cases}$$

$$3V_B + V_C - V_B - V_C = -\frac{1}{L} - \frac{1}{2L} = -\frac{3}{2L}$$

$$V_B = -\frac{3}{4L}$$

$$V_C = \frac{1}{2L} - V_B = \frac{3}{2L^2} + \frac{3}{4L} = \frac{5}{4L}$$



$$1. \Delta \varphi_D^q = \frac{1}{EI_1} \int_0^{2L} \left(-2qL^2 \right) \left(-\frac{3}{4L} x_{3I} \right) dx_{3I} + \frac{1}{EI_1} \int_0^L \left(-q^2 - qL x_{3II} \right) \left(-1 - \frac{1}{2L} x_{3II} \right) dx_{3II}$$

$$+ \frac{1}{EI_1} \int_0^{2L} \left(-q \frac{x_{3III}^2}{2} + qL x_{3III} \right) \left(-\frac{1}{2L} x_{3III} \right) dx_{3III}$$

$$= \frac{1}{EI_1} \left[3qL^3 + \frac{23}{12} qL^3 - \frac{qL^3}{3} \right] = \frac{55qL^3}{12EI_1} = \frac{55 \cdot 20 \cdot 10^3}{12 \cdot 210 \cdot 10^3 \cdot 1963 \cdot 10^{-8}} = 0,022 = 1,29^\circ$$

causato termico:

$$1. \Delta \varphi_D^{\Delta T} = \int_{ABC} x_t H^* dx_3 = x_t \frac{qL}{4} \left(-\frac{3}{2} \right) = \left(-\frac{2x_t \Delta T}{H} \right) \left(-\frac{3}{2} L \right) = \frac{3x_t \Delta T L}{H} = \frac{3 \cdot 15 \cdot 10}{9,20} = 0,0015 = 0,086^\circ$$

$$\Delta \varphi_D^{TOT} = \Delta \varphi_D^q + \Delta \varphi_D^{\Delta T} = 1,29^\circ + 0,086^\circ = 1,37^\circ$$