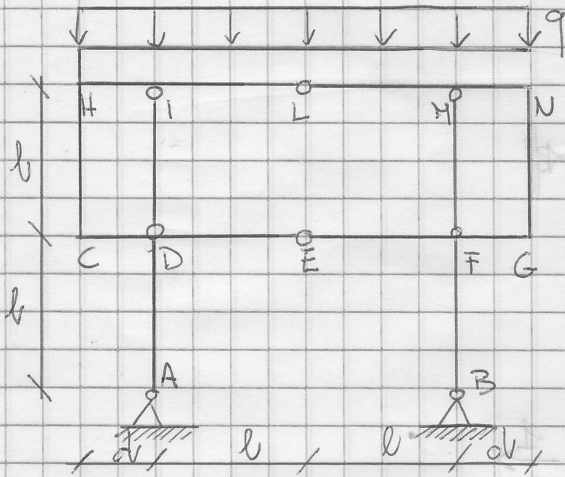
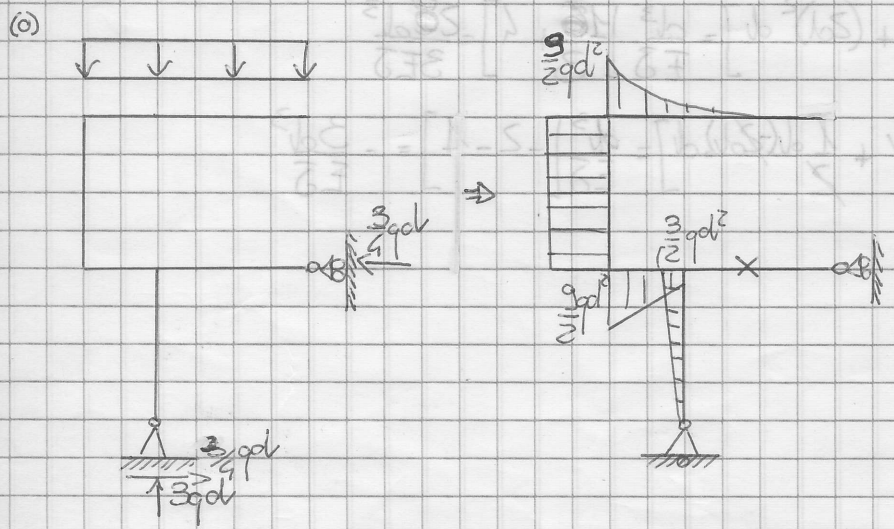
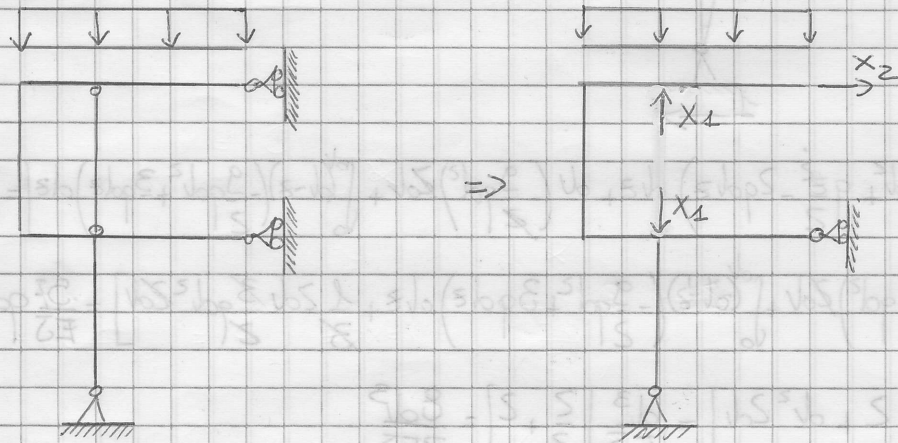


FVA A

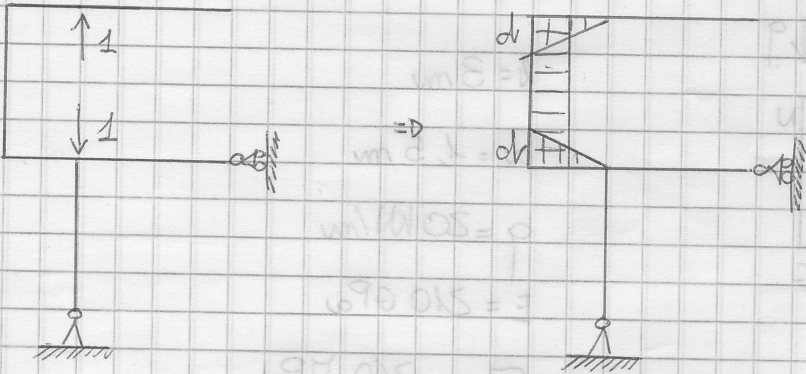


$l = 3 \text{ m}$   
 $d = 1,5 \text{ m}$   
 $q = 20 \text{ kN/m}$   
 $E = 210 \text{ GPa}$   
 $\sigma_{\text{amm}} = 260 \text{ MPa}$

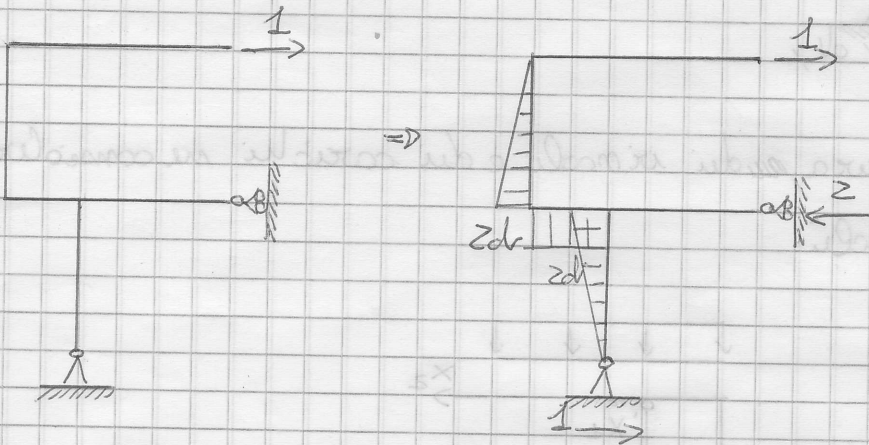
Data la simmetria della struttura, dei vincoli e dei carichi ne considero solo metà con gli opposti vincoli.



(1)



(2)



$$v_{10} = \int \frac{M_1 M_0}{EI} dz = \frac{1}{EI} \int_0^{dv} z \left( -2qdl^2 - qz^2 - 2qdz \right) dz + dv \left( \frac{9qdl^2}{2} \right) Zdv + \int_0^{dv} (dv-z) \left( \frac{9qdl^2}{2} + 3qdz \right) dz = -\frac{3dl^3 qdv}{2EI}$$

$$v_{20} = \int \frac{M_2 M_0}{EI} dz = \frac{1}{EI} \left[ \frac{1}{2} (-Zdv) \left( \frac{9qdl^2}{2} \right) Zdv + \int_0^{dv} (-Zdv) \left( \frac{9qdl^2}{2} + 3qdz \right) dz + \frac{1}{3} Zdv \frac{9qdl^2}{2} Zdv \right] = \frac{17 qdv^4}{EI}$$

$$v_{11} = \int \frac{M_1^2}{EI} dz = \frac{1}{EI} \left[ \frac{1}{3} dv^2 dv \cdot 2 + dv^2 Zdv \right] = \frac{dv^3}{EI} \left[ \frac{2}{3} + 2 \right] = \frac{8dv^3}{3EI}$$

$$v_{22} = \int \frac{M_2^2}{EI} dz = \frac{1}{EI} \left[ \frac{1}{3} (Zdv)^2 Zdv \cdot 2 + (Zdv)^2 dv \right] = \frac{dv^3}{EI} \left[ \frac{16}{3} + 4 \right] = \frac{28dv^3}{3EI}$$

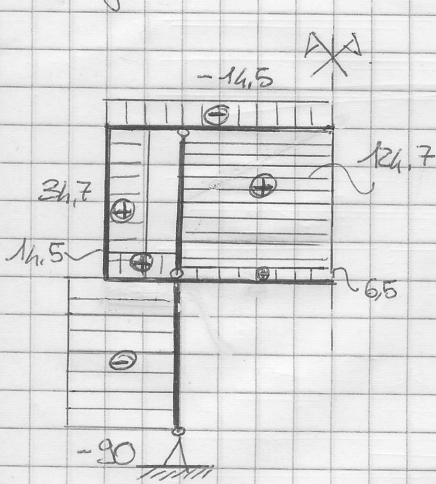
$$v_{12} = \int \frac{M_1 M_2}{EI} dz = \frac{1}{EI} \left[ \frac{1}{2} dv (-Zdv) Zdv + \frac{1}{2} dv (-Zdv) dv \right] = \frac{dv^3}{EI} \left[ -2 - 1 \right] = -\frac{3dv^3}{EI}$$

$$\begin{bmatrix} \frac{8}{3} & -3 \\ -3 & \frac{28}{3} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} \frac{3dl^3 qdv}{2EI} \\ -\frac{17 qdv^4}{EI} \end{bmatrix}$$

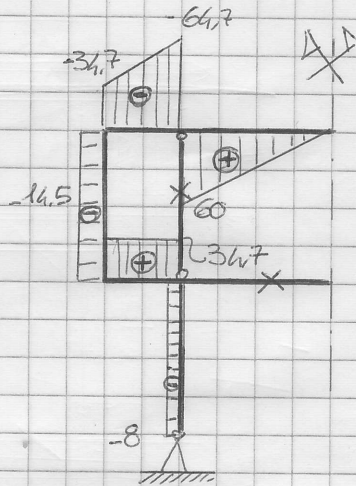
$$X_1 = 124,7 \text{ KN}$$

$$X_2 = -14,5 \text{ KN}$$

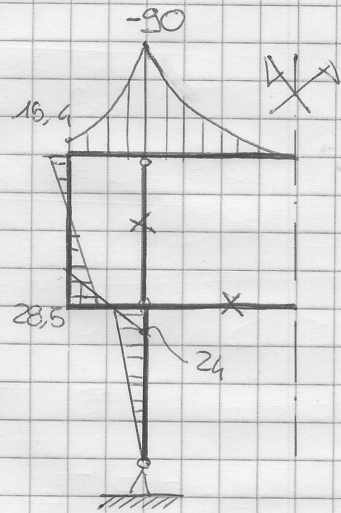
## Grafici delle sollecitazioni



⊕ [kN]



⊕ [kN]



⊕ [kNm]

## Progetto della struttura

$$W_{\min} = \frac{M_{\max}}{\sigma_{\text{amm}}} = \frac{90}{260 \cdot 10^8} \cdot 10^6 = 346,2 \text{ cm}^3 \Rightarrow \text{HEB 180}$$

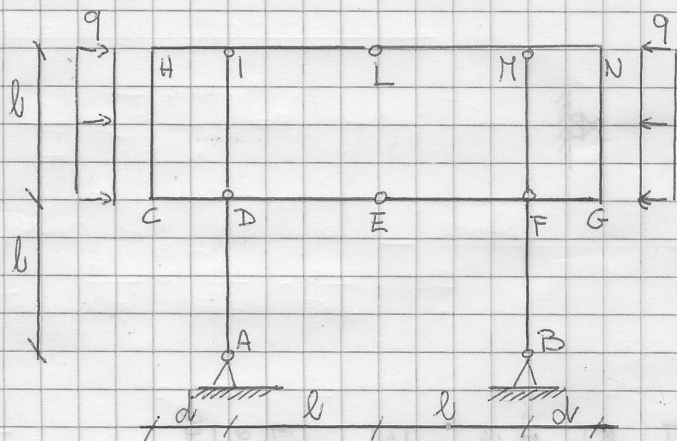
Si considera ora la deformabilità assiale delle aste ID e MF. L'energia termica non nulla è il seguente

$$U_{\text{ass}} = \int_0^{2d} \frac{N_z^2}{EA} dz = \frac{1+2d}{EA}$$

tramite il quale si ricavano i nuovi valori di  $X_1$  e  $X_2$

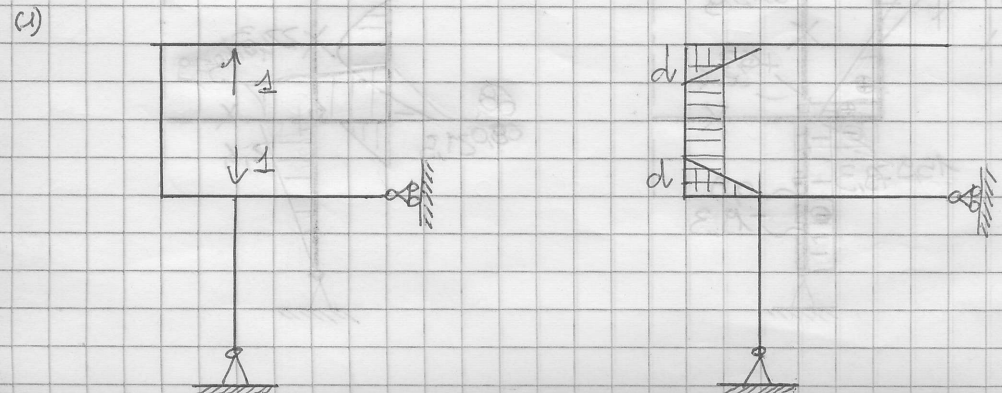
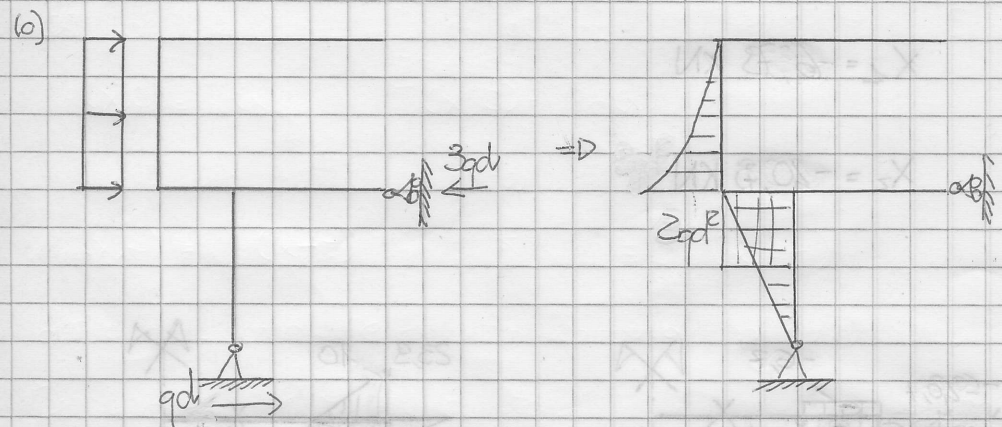
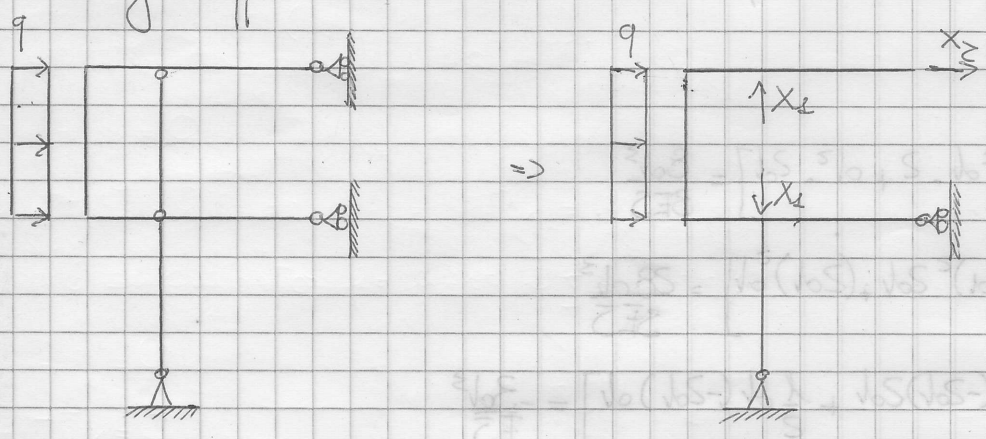
$$\begin{bmatrix} \frac{8+2d}{3} \frac{1}{d^2 A} & -3 \\ -3 & \frac{28}{3} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} \frac{30d}{24} qd \\ -17 qd \end{bmatrix} \quad \begin{matrix} X_1 = 124,66 \text{ kN} \\ X_2 = -14,9 \text{ kN} \end{matrix}$$

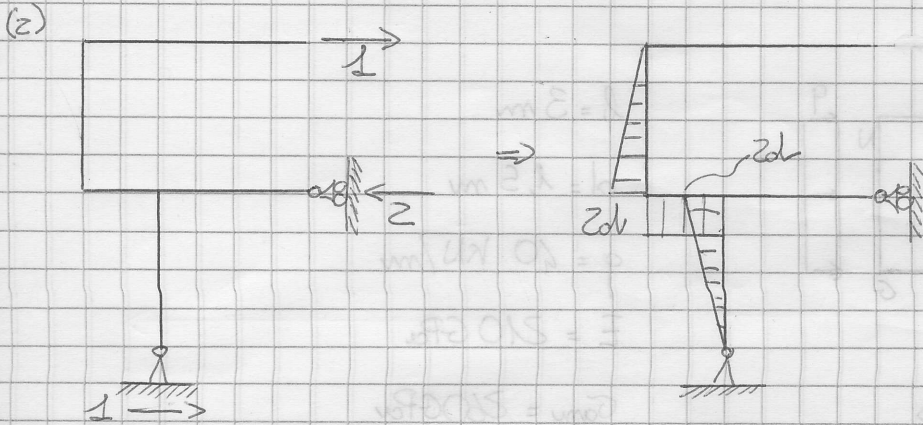
FILA B



$b = 3 \text{ m}$   
 $d = 1,5 \text{ m}$   
 $q = 40 \text{ kN/m}$   
 $E = 210 \text{ GPa}$   
 $\sigma_{amm} = 260 \text{ Pa}$

Data la simmetria della struttura, dei vincoli e dei carichi ne considero solo metà con gli opportuni vincoli.





$$y_{10} = \int_0^l \frac{M_1 M_0}{EI} dz = \frac{1}{EI} \int_0^{2cl} dz \left[ -q \frac{z^2}{2} \right] dz - \frac{1}{EI} \int_{2cl}^l dz \left[ qd^2 dz \right] = \frac{1}{EI} \left[ -\frac{1}{3} qd^3 - qd^3 \right] = -\frac{7}{3} \frac{qd^4}{EI}$$

$$y_{10} = \int_0^l \frac{M_1 M_0}{EI} dz = \frac{1}{EI} \int_0^{2cl} (-3) \left( -q \frac{z^2}{2} \right) dz + \int_{2cl}^l 2cl \cdot 2qd^2 dz + \frac{1}{3} \int_{2cl}^l 2cl \cdot 2qd^2 \cdot 2cl dz = \frac{1}{EI} \left[ 2qd^3 + 4qd^3 + \frac{8}{3} cl^3 \right]$$

$$= \frac{26}{3} \frac{qd^4}{EI}$$

$$y_{11} = \int_0^l \frac{M_1^2}{EI} dz = \frac{1}{EI} \left[ \frac{1}{3} d^2 \cdot d \cdot 2 + d^2 \cdot 2cl \right] = \frac{8}{3} \frac{cd^3}{EI}$$

$$y_{12} = \int_0^l \frac{M_2^2}{EI} dz = \frac{1}{EI} \left[ \frac{1}{3} (2cl)^2 \cdot 2cl + (2cl)^2 \cdot d \right] = \frac{28}{3} \frac{cd^3}{EI}$$

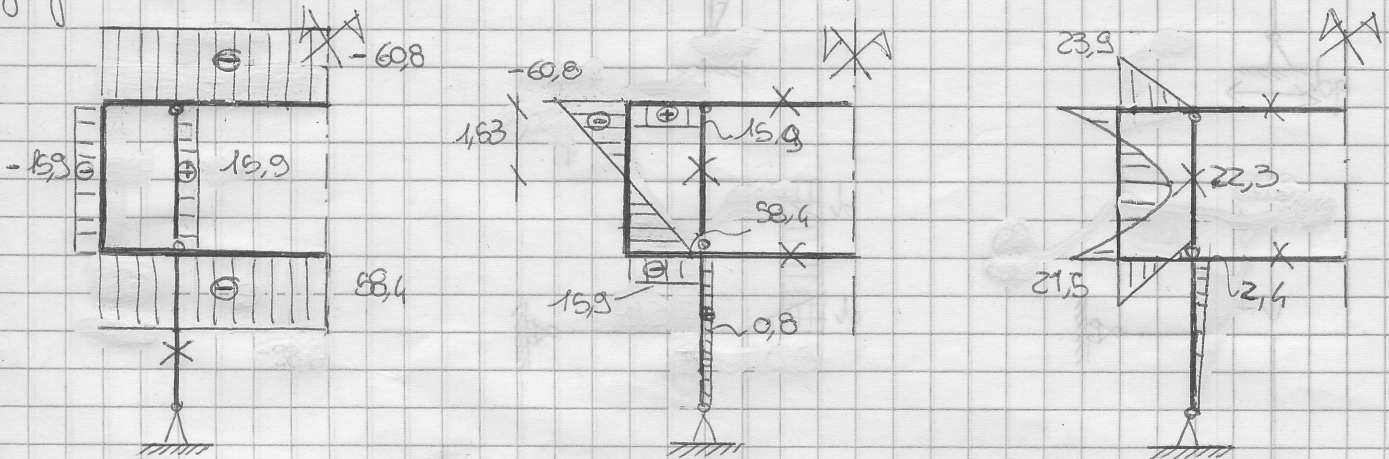
$$y_{12} = \int_0^l \frac{M_1 M_2}{EI} dz = \frac{1}{EI} \left[ \frac{1}{2} d \cdot (-2cl) \cdot 2cl + \frac{1}{2} d \cdot (-2cl) \cdot d \right] = -\frac{3}{EI} cl^3$$

$$\begin{bmatrix} \frac{8}{3} & -3 \\ -3 & \frac{28}{3} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} \frac{7}{3} qd \\ -\frac{28}{3} qd \end{bmatrix}$$

$$X_1 = -15,9 \text{ KN}$$

$$X_2 = -60,8 \text{ KN}$$

Grafici delle sollecitazioni



Progetto della sezione

$$W_{min} = \frac{M_{max}}{\sigma_{amm}} = \frac{23,9 \cdot 10^3}{260 \cdot 10^3} = 91,9 \text{ cm}^3 \Rightarrow \text{IPE 160}$$

Si considera ora la deformabilità assiale delle aste ID e KF. L'unica componente non nulla è la seguente

$$v_{41}^a = \int_0^{2l} \frac{N_2^z}{EA} dz = \frac{1 \cdot 2l}{EA}$$

tramite il quale si ricavano i nuovi valori di  $X_1$  e  $X_2$

$$\begin{bmatrix} \frac{8}{3} + \frac{25}{EA} & -3 \\ -3 & \frac{28}{3} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} \frac{7}{3} \text{ qdl} \\ -\frac{26}{3} \text{ qdl} \end{bmatrix}$$

$$X_1 = -15,92 \text{ kN}$$

$$X_2 = -60,83 \text{ kN}$$