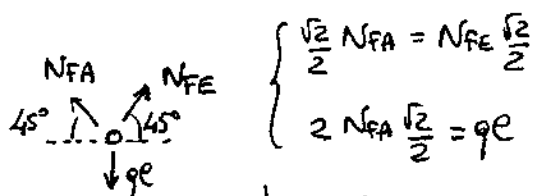


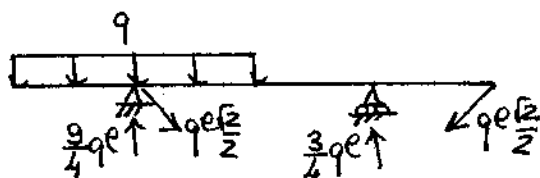
$$\uparrow V_B 2e - qe \frac{3}{2}e = 0 \rightarrow V_B = \frac{3}{4}qe = 1500 \text{ kg}$$

$$V_A = 2qe + qe - \frac{3}{4}qe = \frac{9}{4}qe = 4500 \text{ kg}$$

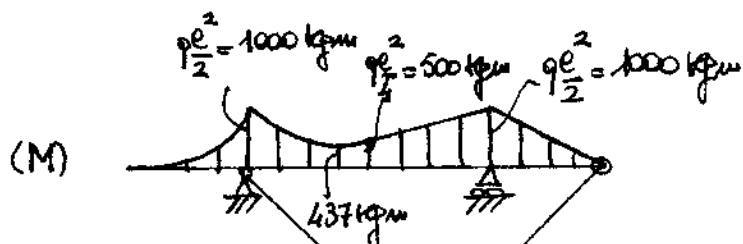
Equilibrio del nodo F:



$$\begin{cases} \frac{\sqrt{2}}{2} N_{FA} = N_{FE} \frac{\sqrt{2}}{2} \\ 2 N_{FA} \frac{\sqrt{2}}{2} = qe \end{cases} \rightarrow N_{FA} = N_{FE} = qe \frac{\sqrt{2}}{2} = 1414 \text{ kg}$$

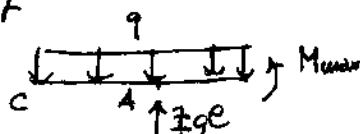
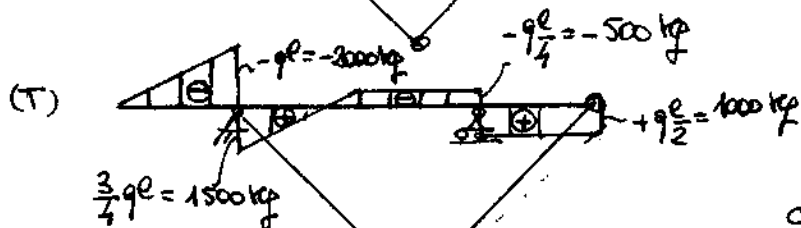


Calcoli:

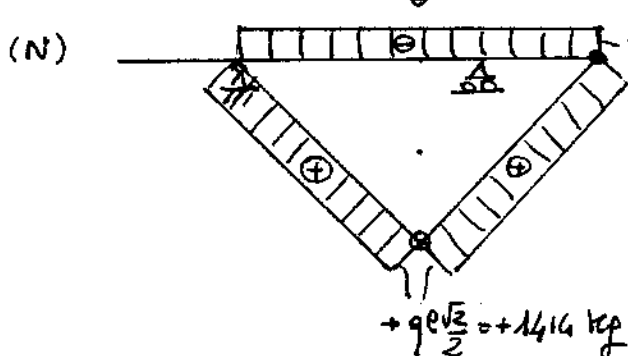


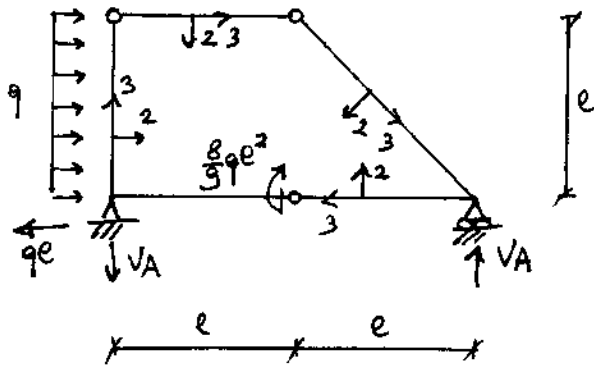
$$qe \downarrow \begin{array}{c} A \\ \uparrow T_A^+ \\ \uparrow \frac{13}{4}qe \end{array} \quad T_A^+ = \left( \frac{9}{4} - \frac{3}{2} \right) qe = \frac{3}{4} qe$$

$$T_B \downarrow \begin{array}{c} B \\ \uparrow \frac{3}{4}qe \end{array} \quad T_B = \frac{qe}{4}$$



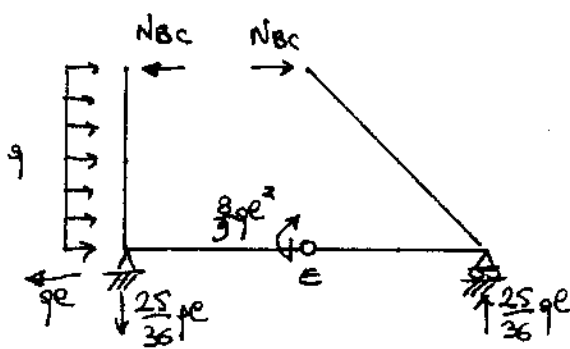
$$M_{max} = -\frac{7}{4} qe \frac{7e}{8} + \frac{7}{4} qe \frac{3e}{4} = -\frac{7}{32} qe^2 = 437 \text{ kgm}$$





$$\uparrow A \quad V_A \cdot 2e - \frac{8}{9} q e^2 - \frac{q e^2}{2} = 0$$

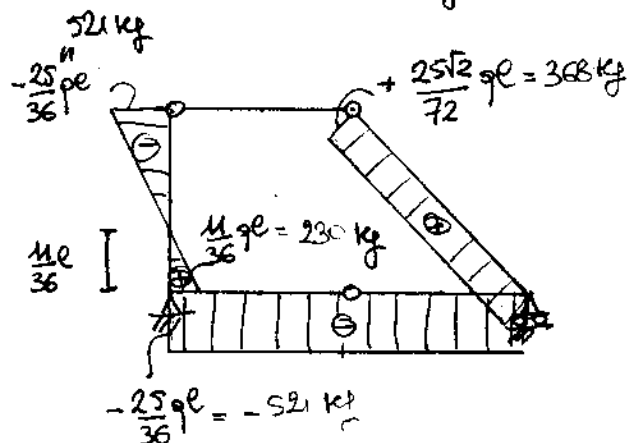
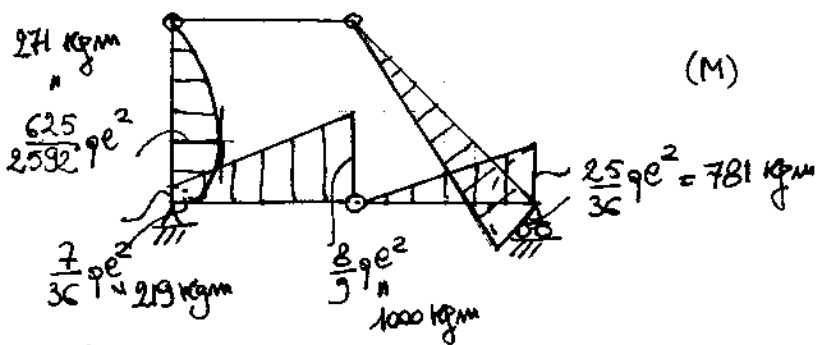
$$\rightarrow V_A = \frac{25}{36} q e = 521 \text{ kg}$$



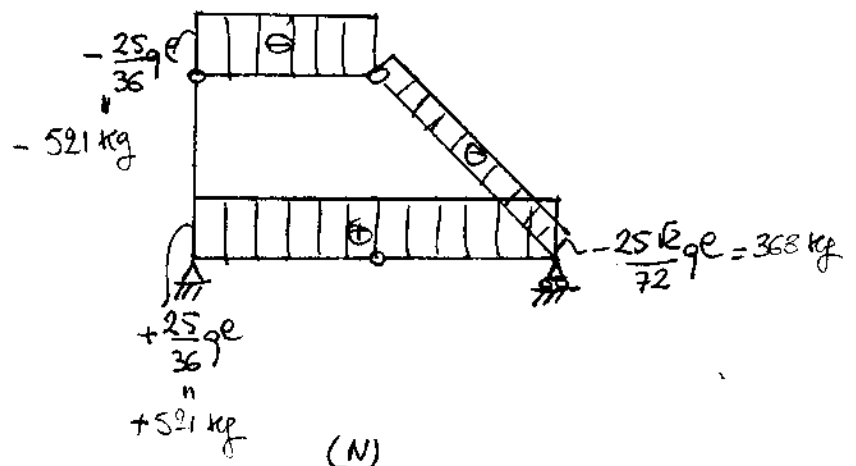
$$\rightarrow -N_{bc} e + \frac{25}{36} q e^2 = 0$$

$$\rightarrow N_{bc} = \frac{25}{36} q e \text{ (compression)} \\ = 521 \text{ kg}$$

Distribuzioni quote:

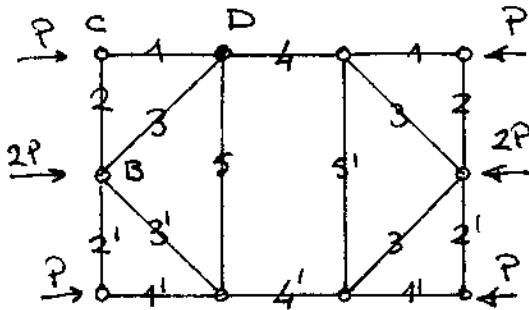


(T)



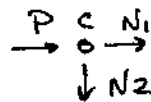
(N)

Stato di sollecitazione primario:



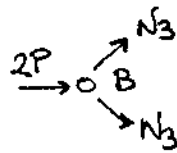
$$P = 90/2 = 375 \text{ kg}$$

La struttura ha due assi di simmetria.  
 È quindi sufficiente considerare  
 l'equilibrio dei soli nodi C, B e D.  
 Per simmetria si ha poi che  $N_2' = N_2$ , etc.



$$N_1 = -P = -375 \text{ kg (pressione)}$$

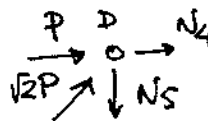
$$N_2 = 0$$



$$2N_3 \frac{\sqrt{2}}{2} = -2P$$

$$\rightarrow N_3 = \sqrt{2}P$$

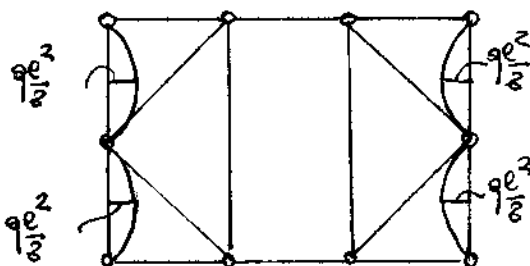
$$= -530 \text{ kg (pressione)}$$



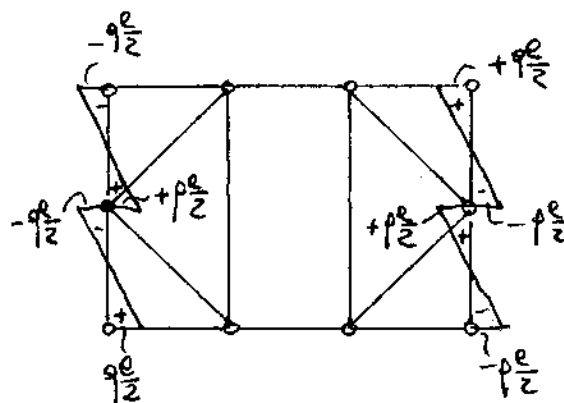
$$N_5 = \sqrt{2}P \frac{\sqrt{2}}{2} = P = 375 \text{ kg (tensione)}$$

$$N_4 = -P - \sqrt{2}P \frac{\sqrt{2}}{2} = -2P = -750 \text{ kg}$$

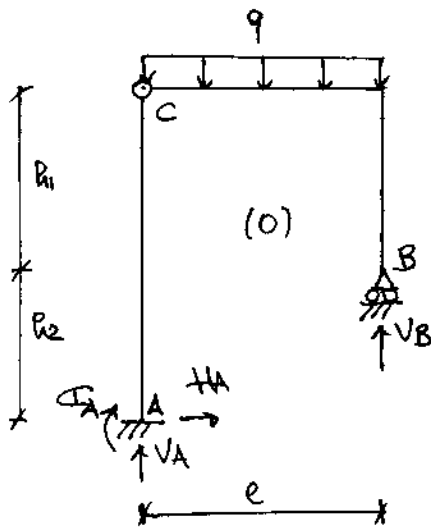
Stato di sollecitazione secondario:



(M)



(T)



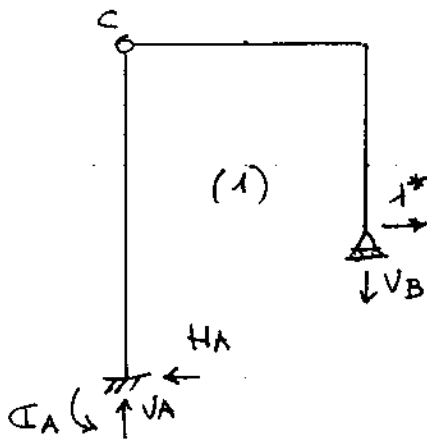
$$H_A = 0$$

$$\curvearrowright \sum \mathcal{M}_A = 0$$

$$\curvearrowright V_B \cdot l - \frac{q l^2}{2} = 0 \rightarrow V_B = \frac{q l}{2}$$

$$V_A = q l - \frac{q l}{2} = \frac{q l}{2}$$

Si applica il teorema dei lavori virtuali prendendo come sistema di spostamenti-deformazioni quello della struttura con il carico  $q$ , e come sistema di forze-tensioni quello agente nella struttura seguente:



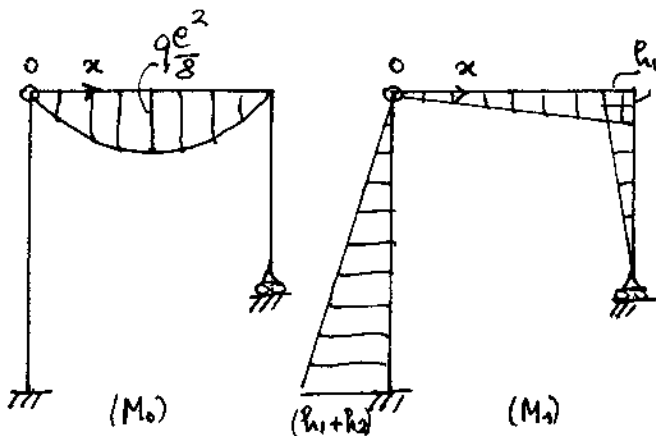
$$H_A = 1$$

$$\curvearrowright -V_B \cdot l + 1 \cdot h_1 = 0 \rightarrow V_B = \frac{h_1}{l}$$

$$V_A = V_B = \frac{h_1}{l}$$

$$\curvearrowright \mathcal{M}_A - H_A (h_1 + h_2) = 0 \rightarrow \mathcal{M}_A = (h_1 + h_2)$$

Diagrammi dei momenti:



Equazione dei lavori virtuali: (\*)

$$EJ \Delta B = \int_0^l \left( \frac{h_1 x}{l} \right) \left( \frac{q l}{2} x - \frac{q x^2}{2} \right) dx$$

$$= \frac{q h_1}{2 l} \int_0^l (l x^2 - x^3) dx$$

$$= \frac{q h_1}{2 l} \left( \frac{l^4}{3} - \frac{l^4}{4} \right) = \frac{q h_1 l^3}{24}$$

$$= 1687.5 \text{ kgcm}^4$$

(\*) Le deformazioni angolari si interpretano trascurabili.