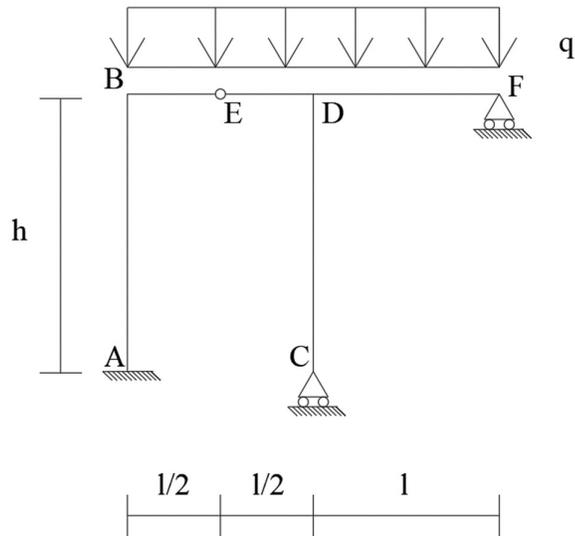
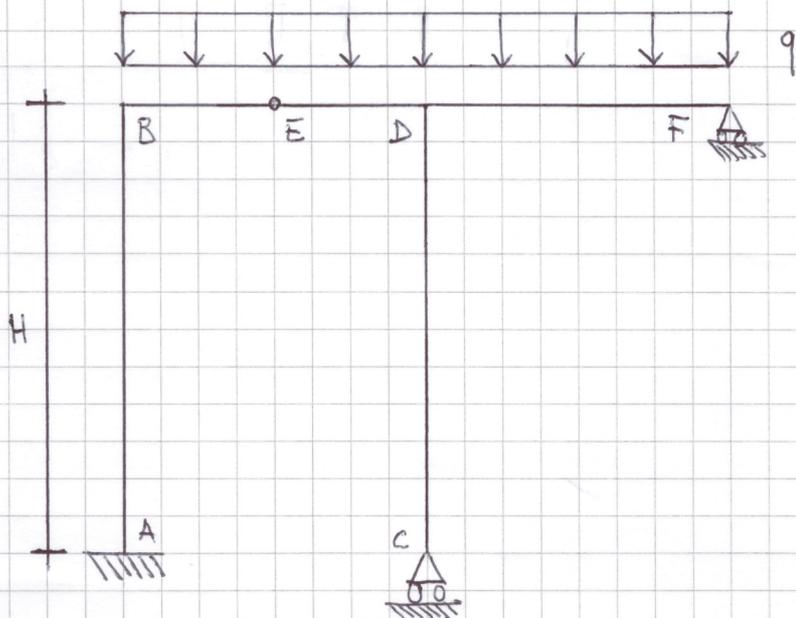


## Totale SdC 21/06/2021



- 1) Determinare i diagrammi quotati MNT della struttura in figura con  $q = 4000$  N/m,  $l = 2$  m,  $h = 3$  m. In questa fase, si trascuri la deformabilità assiale delle aste. Si dimensioni poi a flessione il telaio con la formula  $M/W$  usando profili IPE. Per tutti gli elementi si assuma un acciaio Fe 430 con tensione ammissibile di 190 MPa e modulo di Young pari a 210000 MPa.
- 2) Determinare i diagrammi quotati MNT della struttura considerando il difetto dell'asta CD di 1 cm più lunga e la deformazione assiale.

# SOLUZIONE COMPITO 21/06/2021



DATI:

$$l = 2 \text{ m}$$

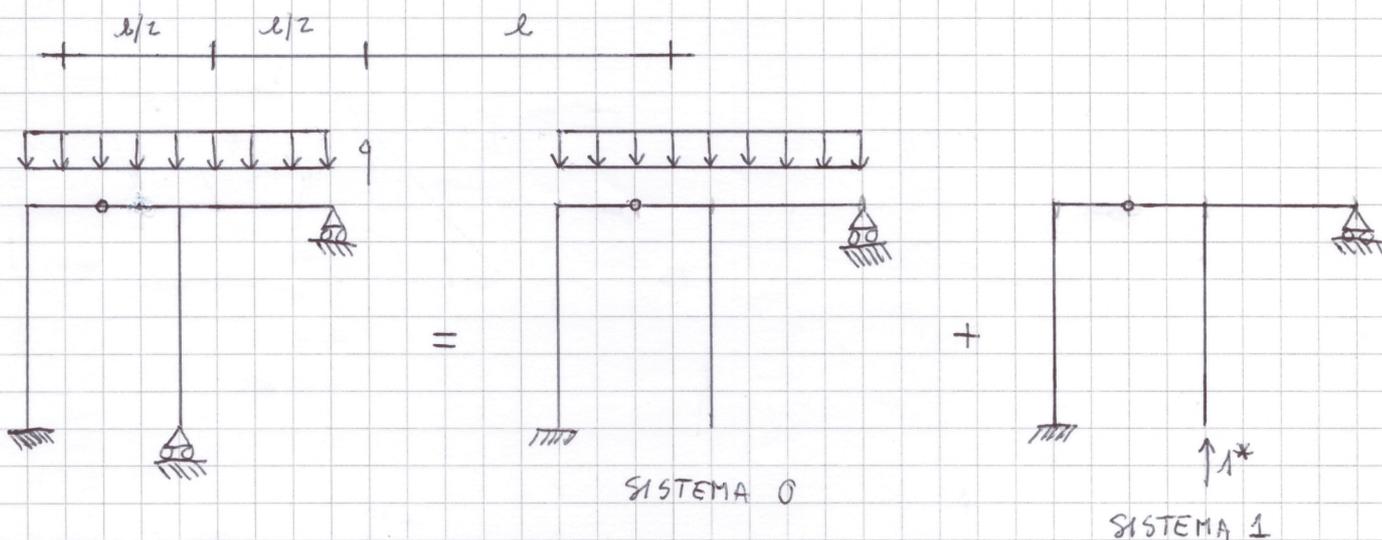
$$H = 3 \text{ m}$$

$$q = 4000 \text{ N/m}$$

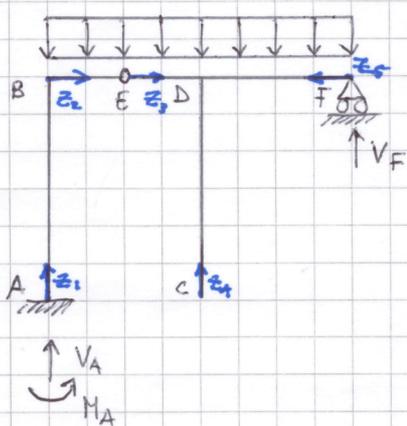
$$E = 210000 \text{ MPa}$$

$$\sigma_{am} = 190 \text{ MPa}$$

$$\Delta H = 1 \text{ cm}$$



1) Si trascuri la deformabilità assiale



SISTEMA 0

$$\rightarrow) H_A = 0$$

$$\overset{E}{\uparrow} \sum_{Dx} V_F \left( l + \frac{l}{2} \right) - q \left( l + \frac{l}{2} \right) \left( \frac{3}{4} l \right) = 0 \rightarrow V_F = \frac{3}{4} q l = 6000 \text{ N}$$

$$\uparrow) V_A + V_F = 2 q l \rightarrow V_A = \frac{5}{4} q l = 10000 \text{ N}$$

$$\overset{E}{\uparrow} \sum_{Sx} -V_A \frac{l}{2} + q \frac{l}{2} \cdot \frac{l}{4} + M_A = 0 \rightarrow M_A = \frac{q l^2}{2} = 8000 \text{ Nm}$$

Tratto AB

$$N(z_1) = -\frac{5}{4} q l = -10000 \text{ N}$$

$$T(z_1) = 0$$

$$M(z_1) = -\frac{q l^2}{2} = -8000 \text{ Nm}$$

Tratto BE

$$N(z_2) = 0$$

$$T(z_2) = \frac{5}{4} q l - q z$$

$$M(z_2) = -\frac{q l^2}{2} + \frac{5}{4} q l z - \frac{q z^2}{2}$$

Tiatto ED

$$N(z_3) = 0$$

$$T(z_3) = \frac{3}{4}ql - ql$$

$$M(z) = \frac{3}{4}qlz - \frac{ql^2}{2}$$

Tiatto CD

$$N(z_4) = 0$$

$$T(z_4) = 0$$

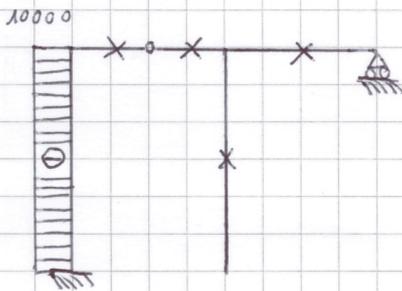
$$M(z_4) = 0$$

Tiatto FD

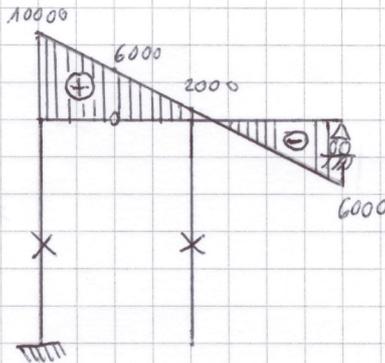
$$N(z_5) = 0$$

$$T(z_5) = -\frac{3}{4}ql + ql$$

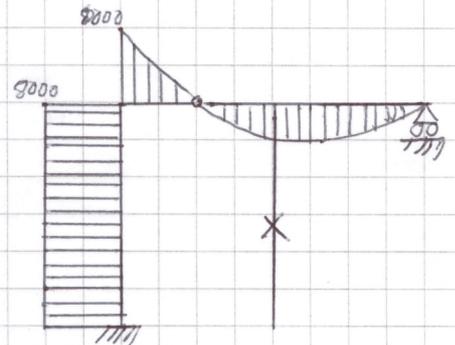
$$M(z_5) = \frac{3}{4}qlz - \frac{ql^2}{2}$$



N [N]

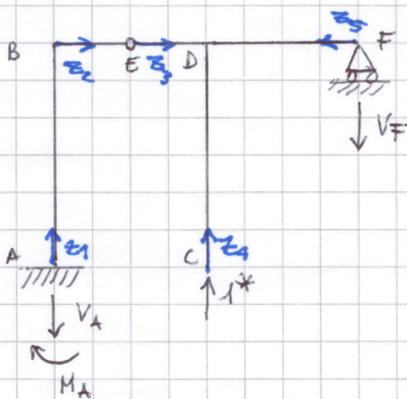


T [N]



M [N.m]

SISTEMA 1



$$\rightarrow) H_A = 0$$

$$\uparrow)_{Dx} -V_F\left(\frac{l}{2}+l\right) + 1*\frac{l}{2} = 0 \rightarrow V_F = \frac{1}{3}$$

$$\uparrow) 1* - V_F - V_A = 0 \rightarrow V_A = 1 - \frac{1}{3} = \frac{2}{3}$$

$$\uparrow)_{Sx} -M_A + V_A\frac{l}{2} = 0 \rightarrow M_A = \frac{1}{3}l = \frac{2}{3}$$

Tiatto AB

$$N(z_1) = \frac{2}{3}$$

$$T(z_1) = 0$$

$$M(z_1) = \frac{2}{3}$$

Tiatto BE

$$N(z_2) = 0$$

$$T(z_2) = -\frac{2}{3}$$

$$M(z_2) = \frac{2}{3} - \frac{2}{3}z$$

Tiatto ED

$$N(z_3) = 0$$

$$T(z_3) = -\frac{2}{3}$$

$$M(z_3) = -\frac{2}{3}z$$

Tiatto CD

$$N(z_4) = -1$$

$$T(z_4) = 0$$

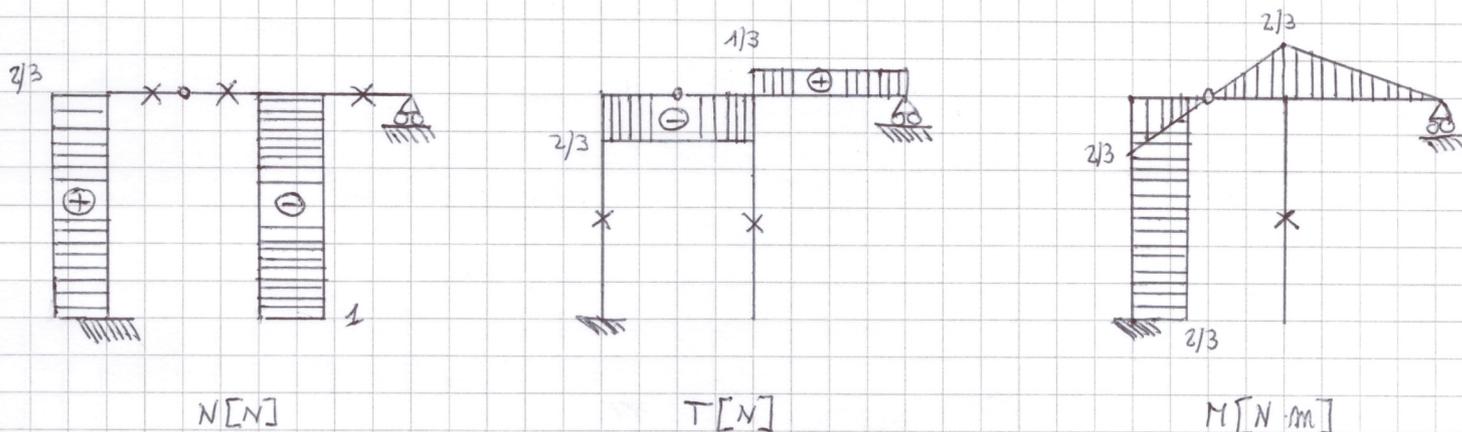
$$M(z_4) = 0$$

Tutte FD

$$N(z_5) = 0$$

$$T(z_5) = 1/3$$

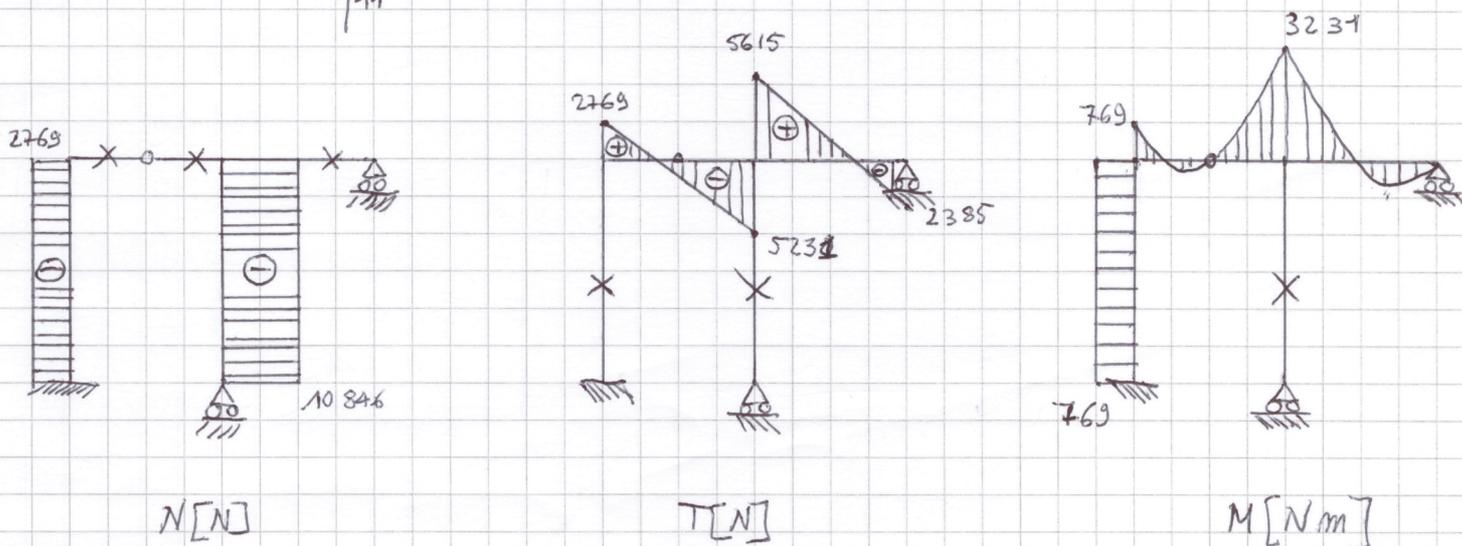
$$M(z_5) = -\frac{1}{3}z$$



$$\eta_{10} = \frac{1}{EJ} \left[ \int_0^H \left( \frac{2}{3} \right) \left( -\frac{qz^2}{2} \right) dz + \int_0^{L/2} \left( \frac{L}{3} - \frac{2}{3}z \right) \cdot \left( -\frac{qz^2}{2} + \frac{5}{4}qLz - \frac{qz^4}{2} \right) dz + \int_0^{L/2} \left( \frac{3}{4}qLz - \frac{qz^2}{2} \right) \cdot \left( -\frac{L}{3}z \right) dz + \int_0^L \left( -\frac{1}{3}z \right) \left( \frac{3}{4}qLz - \frac{qz^2}{2} \right) dz \right] = -\frac{188000}{9EJ}$$

$$\eta_{11} = \frac{1}{EJ} \left[ \int_0^H \left( \frac{2}{3} \right)^2 dz + 2 \int_0^{L/2} \left( -\frac{L}{3}z \right)^2 dz + \int_0^L \left( -\frac{1}{3}z \right)^2 dz \right] = \frac{52}{27EJ}$$

$$X_1 = -\frac{\eta_{10}}{\eta_{11}} = 10846 \text{ N}$$



Progetto a var fissa a flessione

$$M_{max} = 3231 \text{ Nm}$$

$$\frac{M_{max}}{W} < \sigma_{amm} \rightarrow W_{min} = \frac{M_{max}}{\sigma_{amm}} = 17.00 \text{ cm}^3$$

Acciaio profilo IPE 80 ( $A = 7.64 \text{ cm}^2$   $I_x = 80.1$   $W_x = 20.0 \text{ cm}^3$ )

$$\sigma_{mm, \max} = \pm \frac{M}{W_x} \begin{cases} \sigma_{\max} = 162 < 190 \quad \checkmark \\ \sigma_{\min} = -162 < 190 \quad \checkmark \end{cases}$$

2) Considero oggetto asta CD di 1 cm per lunghezza e deformatela lateralmente

$$\eta_{10} = \frac{1}{EJ} \left[ \int_0^{H_{new}} \left(\frac{z}{3}\right) \left(-\frac{9z^2}{2}\right) dz + \int_0^{l/2} \left(\frac{z}{3} - \frac{2}{3}z\right) \left(-\frac{9z^2}{2} + \frac{5}{4}q_l z - \frac{9z^2}{2}\right) dz + \int_0^{l/2} \left(-\frac{2}{3}z\right) \left(\frac{3}{4}q_l z - \frac{9z^2}{2}\right) dz + \int_0^l \left(-\frac{1}{3}z\right) \left(\frac{3}{4}q_l z - \frac{9z^2}{2}\right) dz \right] = -\frac{188480}{9EJ}$$

$$\eta_{11} = \frac{1}{EJ} \left[ \int_0^{H_{new}} \left(\frac{z}{3}\right)^2 dz + 2 \int_0^{l/2} \left(-\frac{2}{3}z\right)^2 dz + \int_0^l \left(-\frac{1}{3}z\right)^2 dz \right] = \frac{1303}{675EJ}$$

$$\eta_{10}^a = \frac{1}{EA} \int_0^{H_{new}} \left(\frac{z}{3}\right) \left(-\frac{5}{4}q_l\right) dz = -\frac{60200}{3EA}$$

$$\eta_{11}^a = \frac{1}{EA} \left[ \int_0^{H_{new}} \left(\frac{z}{3}\right)^2 dz + \int_0^l (-1)^2 dz \right] = \frac{3913}{900EA}$$

$$X_1 = -\frac{\eta_{10} + \eta_{10}^a}{\eta_{11} + \eta_{11}^a} = 10834 \text{ N}$$

