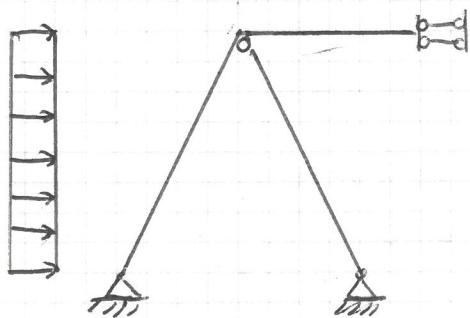
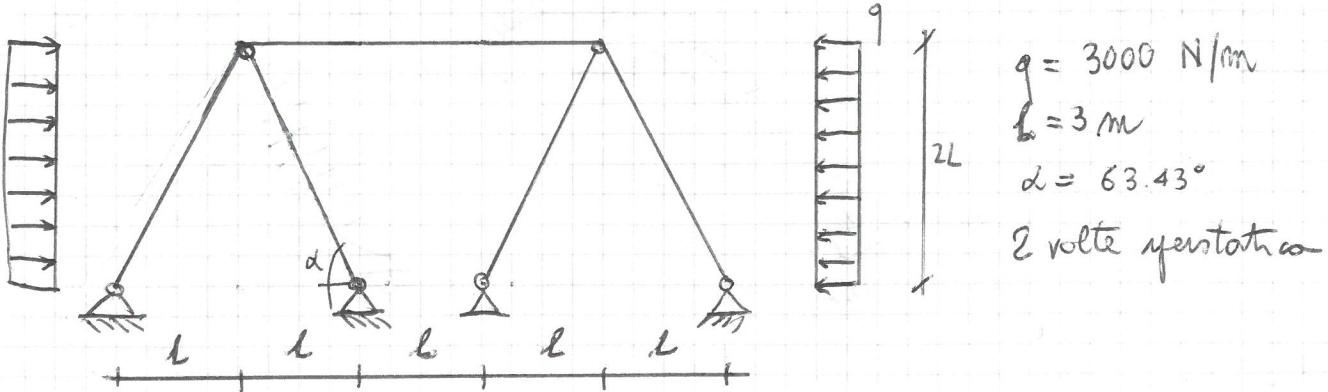
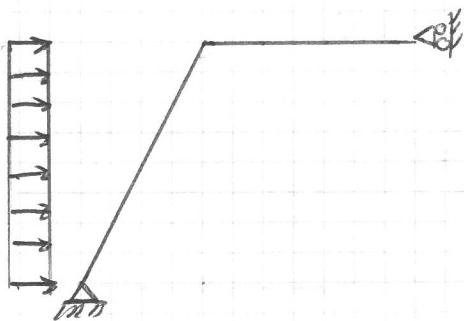


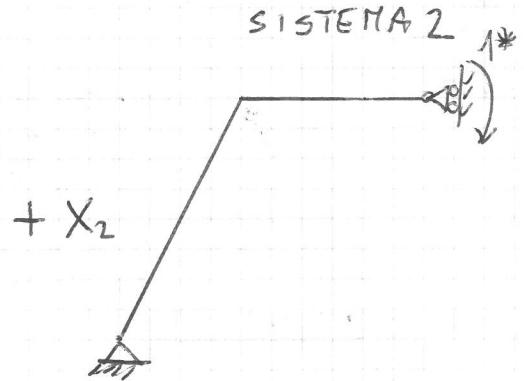
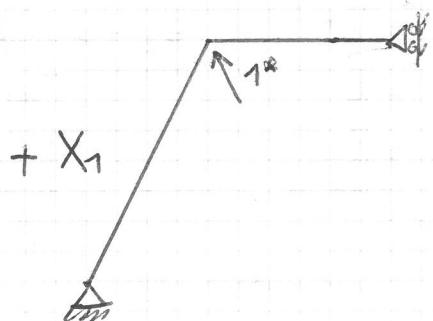
TOTALE



SISTEMA 0



SISTEMA 1

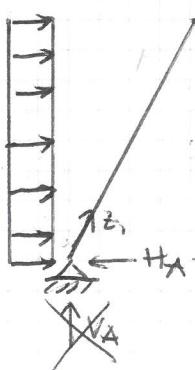


SISTEMA 0

$$A) -2q l \cdot l + H_G \cdot 2l = 0 \rightarrow H_G = ql = 9000 \text{ N}$$

$$H_A = H_G$$

$$V_A = 0$$



$$z_1 \rightarrow N(z_1) = H_A \cos \alpha - q \sin \alpha \cos \alpha z$$

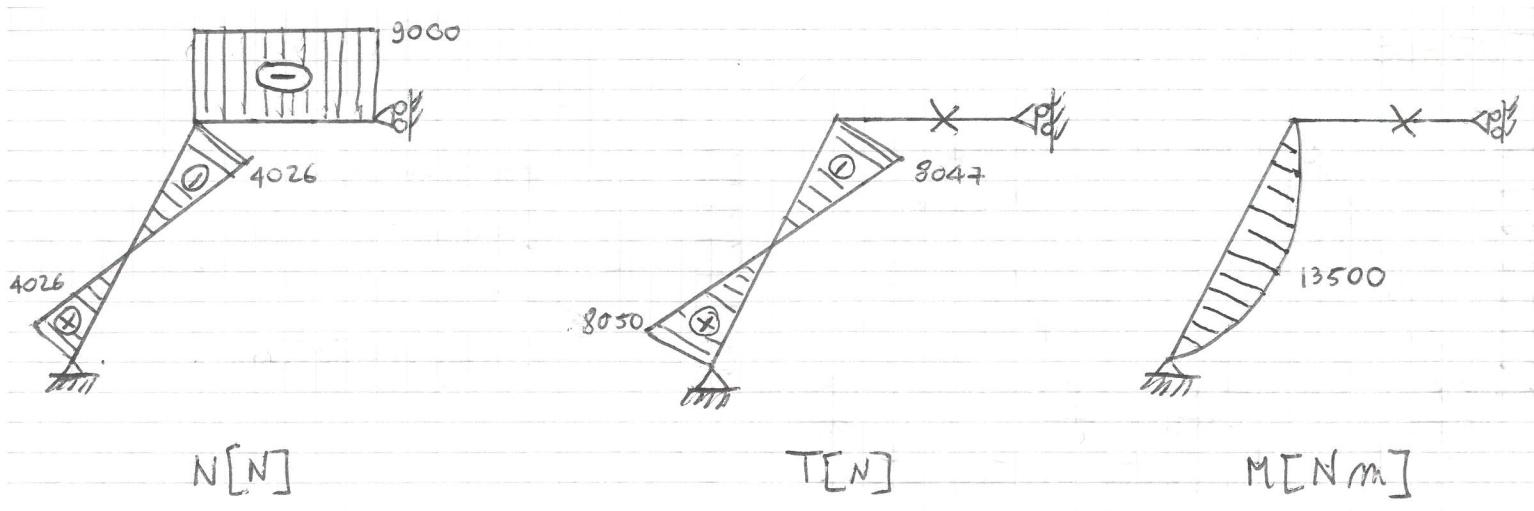
$$T(z_1) = H_A \sin \alpha - q \sin^2 \alpha z$$

$$M(z_1) = H_A \sin \alpha z - q \sin^2 \alpha \frac{z^2}{2}$$

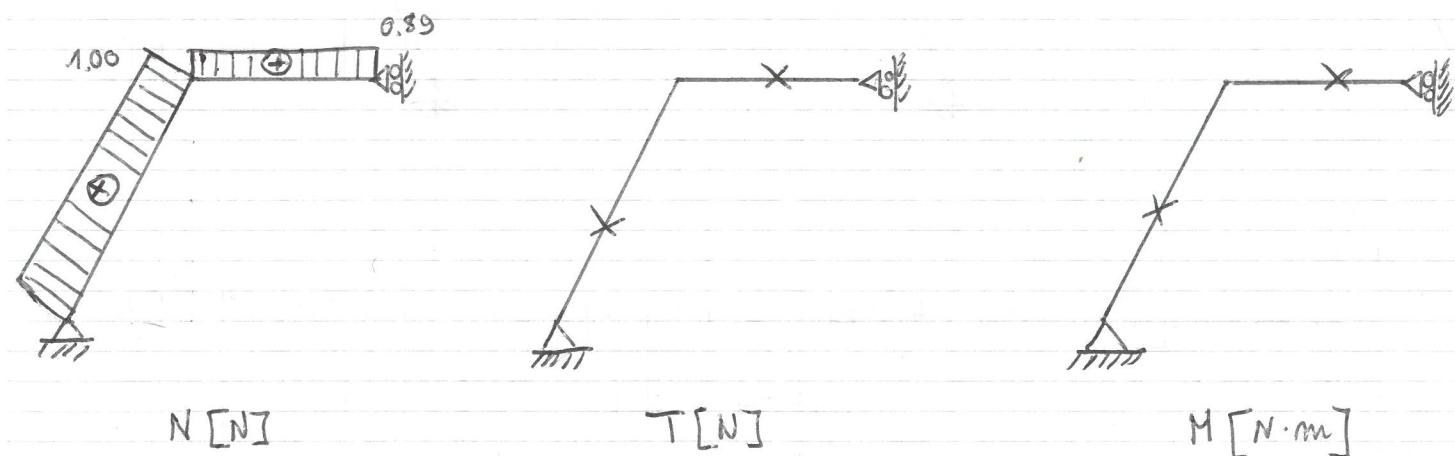
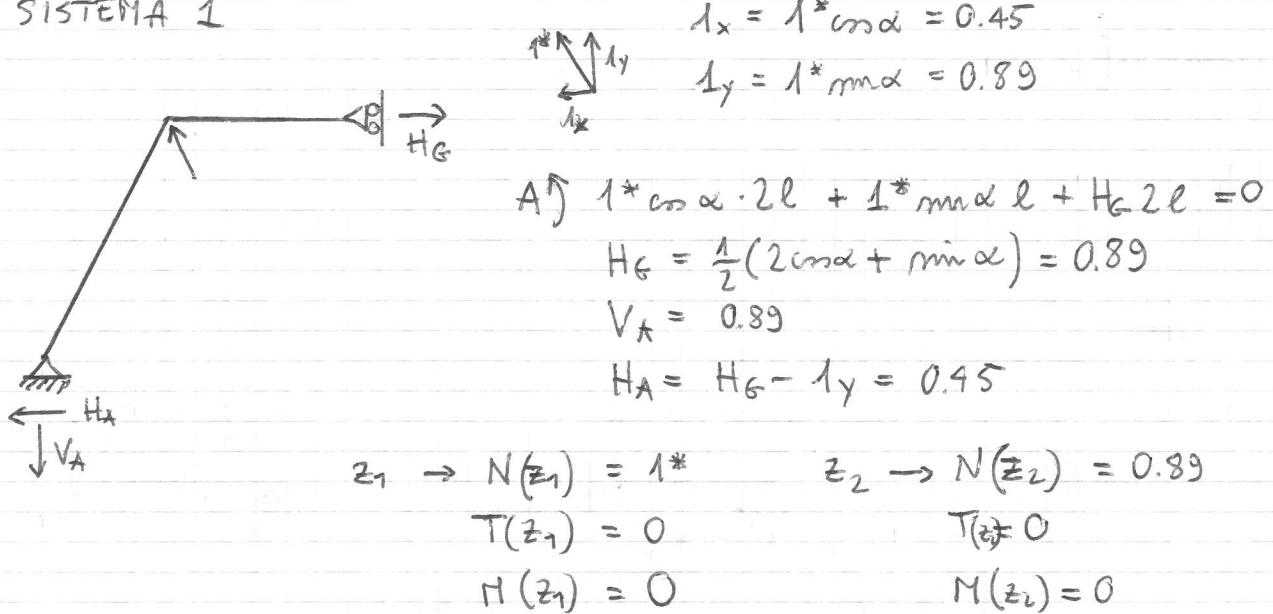
$$z_2 \rightarrow N(z_2) = -ql = -9000 \text{ N}$$

$$T(z_2) = 0$$

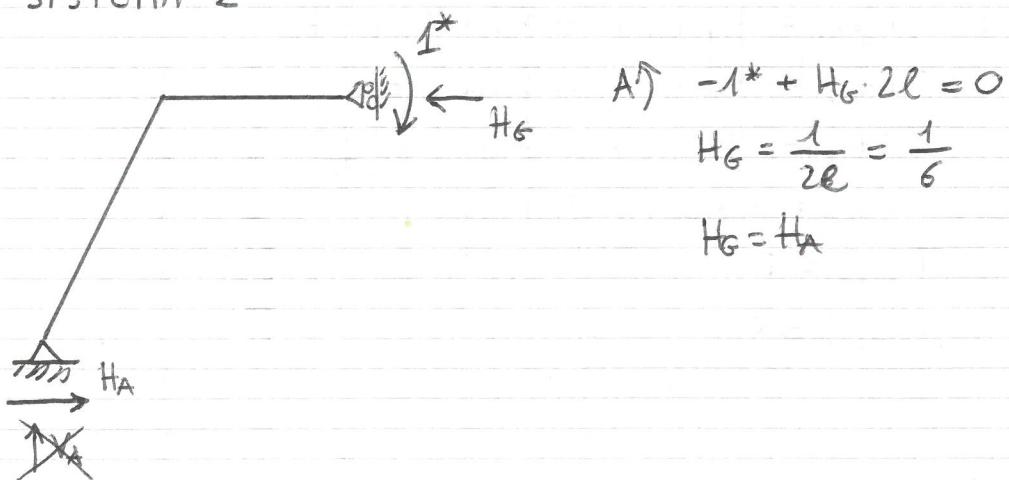
$$M(z_2) = 0$$



SISTEMA 1



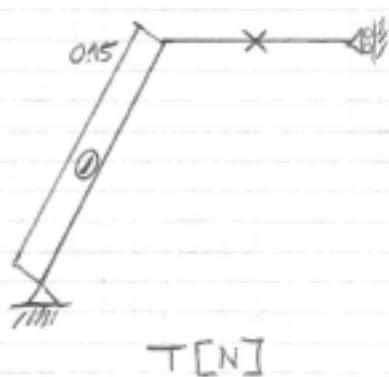
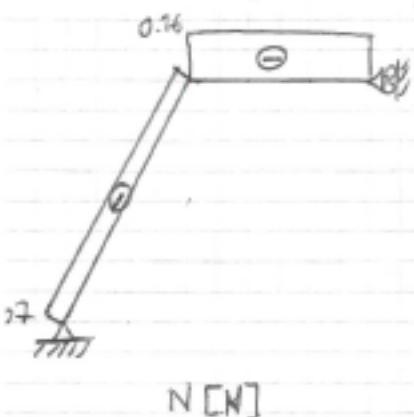
SISTEMA 2



$$z_1 \rightarrow N(z_1) = -\frac{1}{6} \text{ mm} \alpha = -0.07 \text{ N}$$

$$T(z_1) = -\frac{1}{6} \text{ mm} \alpha = -0.15 \text{ N}$$

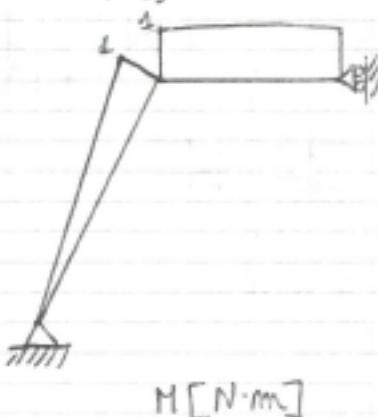
$$M(z_1) = -\frac{1}{6} \text{ mm} \alpha z$$



$$z_L \rightarrow N(z_L) = -1/6$$

$$T(z_L) = 0$$

$$M(z_L) = -1$$



$$\eta_{10} = 0$$

$$\eta_{20} = \frac{1}{EI} \left[\int (-\frac{1}{6} \text{ mm} \alpha z) \left(H_A \text{ mm} \alpha z - q \text{ mm}^2 \frac{z^2}{2} \right) dz = -\frac{30185}{EI} \right]$$

$$\eta_{11} = 0$$

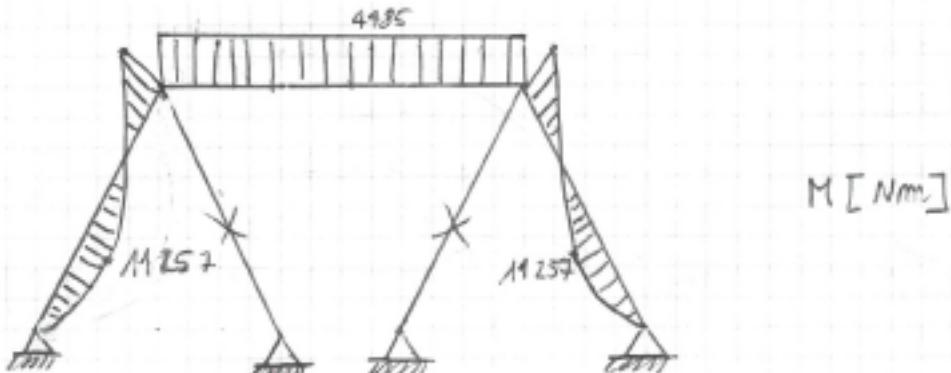
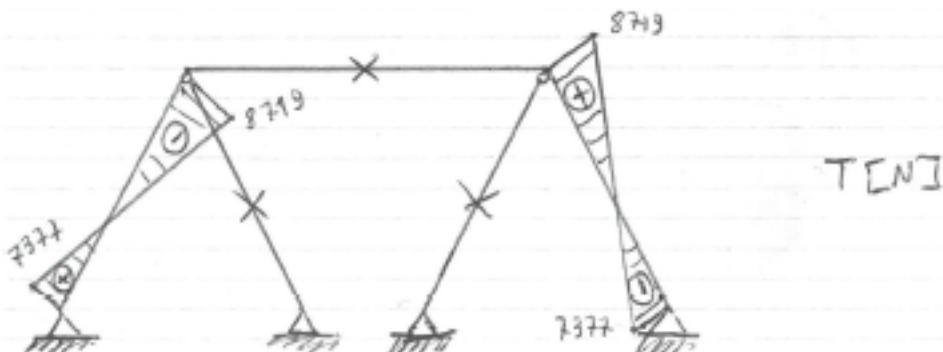
$$\eta_{21} = \frac{1}{EI} \left[\int \left(-\frac{1}{6} \text{ mm} \alpha z \right)^2 dz + \int (-1)^L dz = \frac{6.73}{EI} \right]$$

$$\eta_{21} = 0$$

$$\begin{vmatrix} \eta_{11} & \eta_{21} \\ \eta_{21} & \eta_{22} \end{vmatrix} \begin{vmatrix} x_1 \\ x_2 \end{vmatrix} = \begin{vmatrix} -\eta_{10} \\ -\eta_{20} \end{vmatrix}$$

x_1 e indeterminato

$$x_2 = 4485 \text{ N} \cdot \text{m}$$



$$2) M = 11357 \text{ N}$$

$$T = 0 \text{ N}$$

$$N = 0 \text{ N}$$

$$\sigma_{\text{ann}} = 190 \text{ N/mm}^2$$

$$E = 210000 \text{ MPa}$$

$$W_{\text{min}} = \frac{M}{\sigma_{\text{ann}}} = \frac{11357}{190} = 59.86 \text{ cm}^3$$

Adatto IPE 140 $A = 16.43 \text{ cm}^2$ $J_x = 541.2 \text{ cm}^4$ $W = 77.32 \text{ cm}^3$

$$\underline{\sigma}_z = \pm \frac{M}{W} = \begin{cases} +147 \text{ N/mm}^2 < \sigma_{\text{ann}} & \checkmark \\ -147 \text{ N/mm}^2 < \sigma_{\text{ann}} & \checkmark \end{cases}$$

3) DEFORMABILITÀ ASSIALE BIELLA

$$\eta_{11}^{\text{NEW}} = \eta_{11}^{\text{OLD}} + \eta_{11}^{\text{biella}} = 0 + \int_0^{3/\text{cm}(a)} (-1)^2 / EA \, dz = \frac{6707}{EA}$$

DEFORMABILITÀ ASSIALE BIELLA + CARICO TERMICO

$$\begin{cases} \eta_{11}^{\text{NEW}} X_1 + \eta_{12} X_2 + \eta_{10} + \int_0^{3/\text{cm}(a)} \alpha \Delta T (-1) = 0 \\ \eta_{12} X_1 + \eta_{22} X_2 + \eta_{20} = 0 \end{cases}$$

$$X_1 = 82808 \text{ N}$$

$$X_2 = 4485 \text{ N} \cdot \text{m}$$

