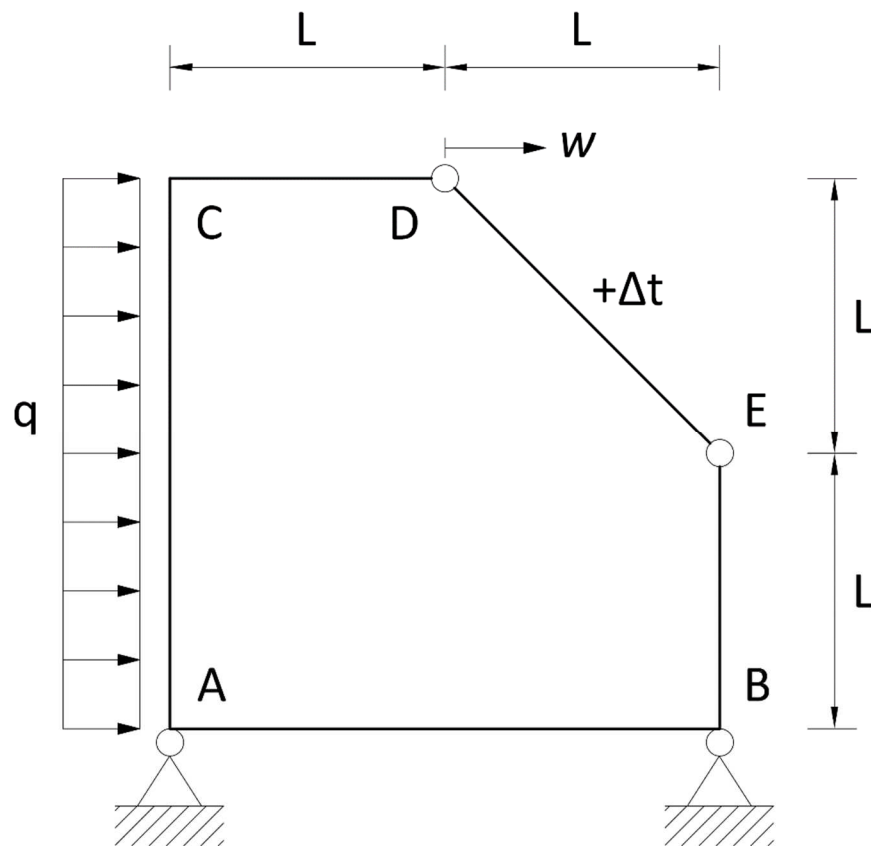
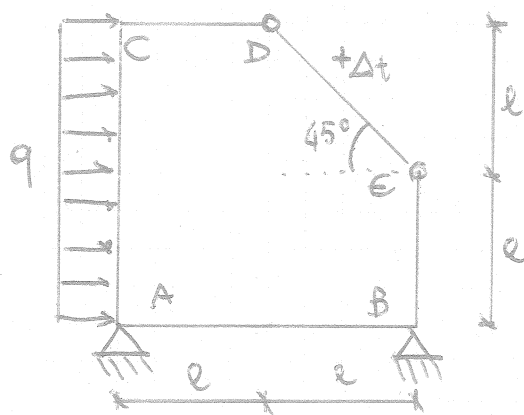




- 1) Risolvere la struttura in figura mediante il metodo delle forze e disegnare i diagrammi M,N,T avendo posto $L=3\text{m}$, $q=2000\text{ N/m}$. In questa fase è lecito trascurare la deformazione assiale delle aste e il carico termico sull'asta DE.
- 2) Progettare il telaio alle tensioni ammissibili mediante profilati IPE assumendo un acciaio con tensione ammissibile di progetto pari a 390 MPa, modulo di Young $E=210000\text{ MPa}$ e considerando la tensione normale massima calcolata al punto 1.
- 3) Risolvere e determinare i diagrammi M,N,T tenendo conto della deformabilità assiale delle aste e considerando il carico termico $\Delta t=30^\circ\text{C}$ sull'asta DE (coefficiente di dilatazione termica $\alpha=1,2 \times 10^{-5} \text{ }^\circ\text{C}^{-1}$).
- 4) Calcolare lo spostamento orizzontale w del nodo D in assenza della deformabilità assiale.

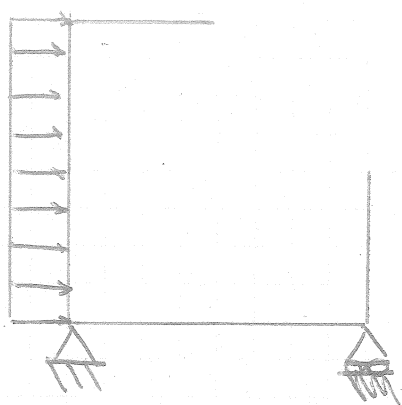
FILA A

06/06/2017

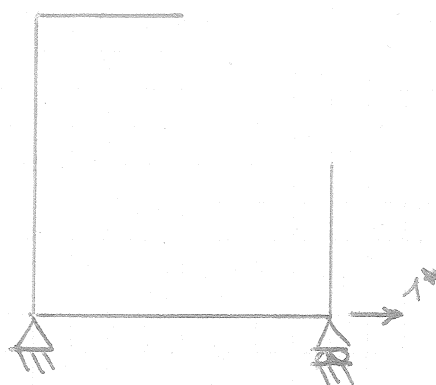


$$l = 3\text{m}$$

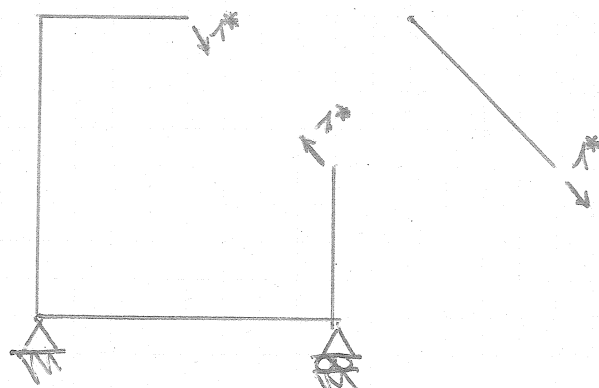
$$q = 2000\text{ N/m}$$



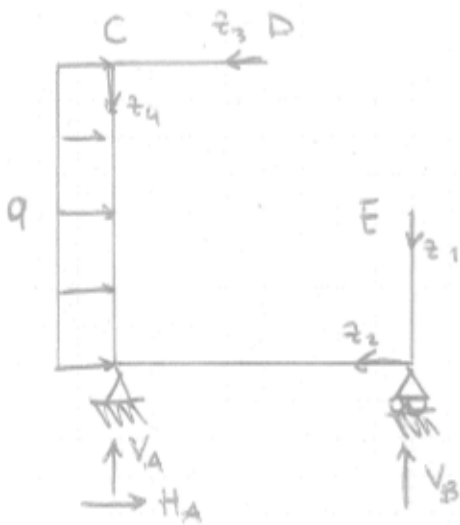
+ X_1



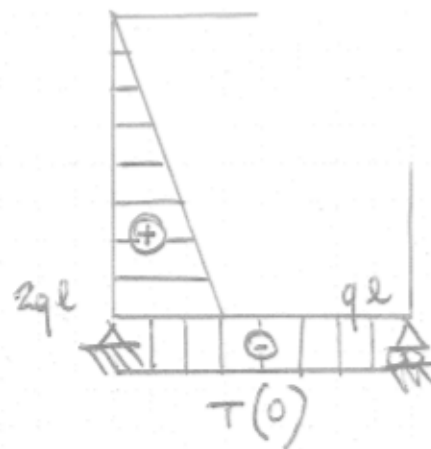
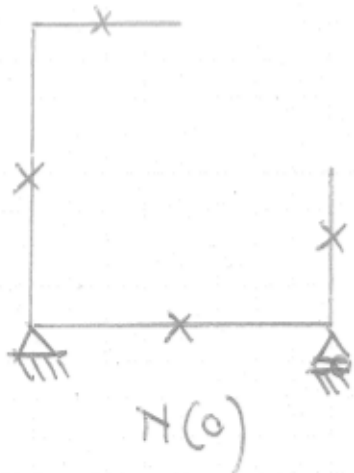
+ X_2



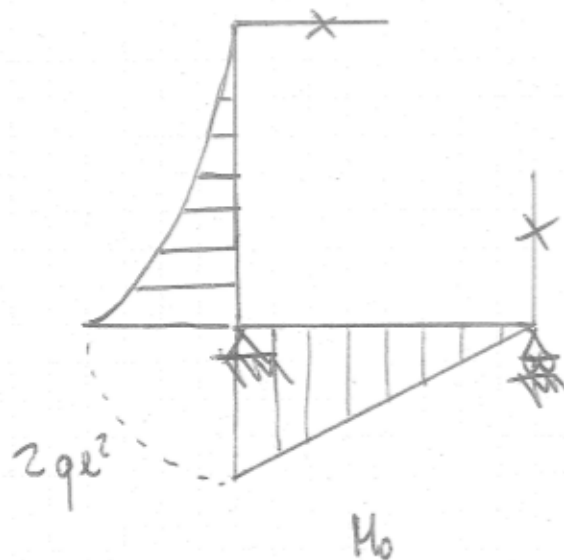
1) SISTEMA (0)



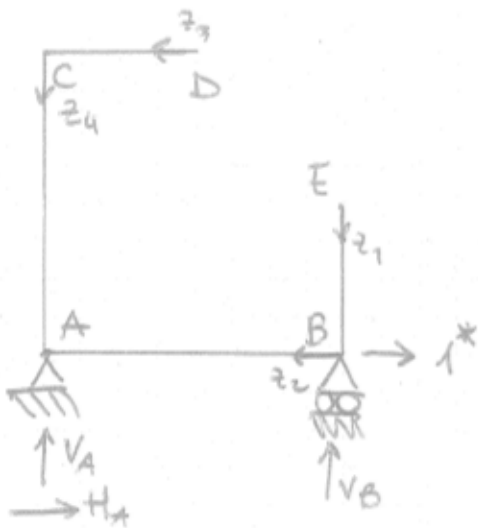
$$\begin{aligned} \rightarrow) H_A &= -2ql \\ \uparrow) V_B \cdot 2l - q2l^2 &= 0 \\ V_B &= ql \\ \uparrow) V_A &= -V_B = -ql \end{aligned}$$



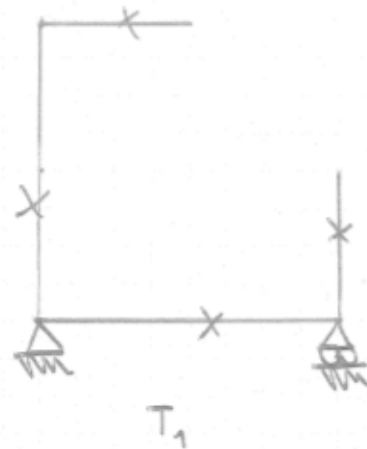
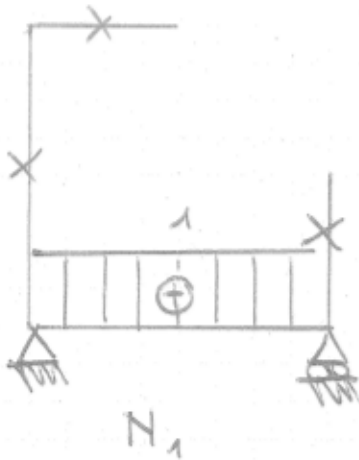
$$\begin{aligned} M_D(z_1) &= 0 \\ M_O(z_2) &= V_B \cdot z = qlz \\ M_O(z_3) &= 0 \\ M_O(z_4) &= -\frac{qz^2}{2} \end{aligned}$$



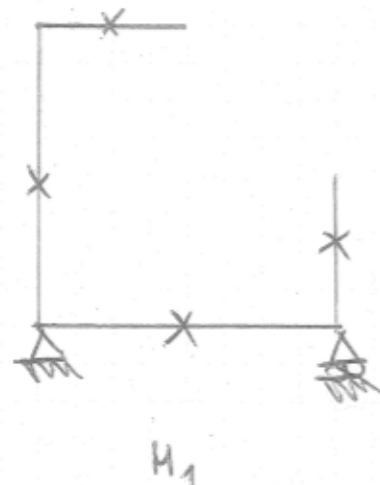
SISTEMA (1)



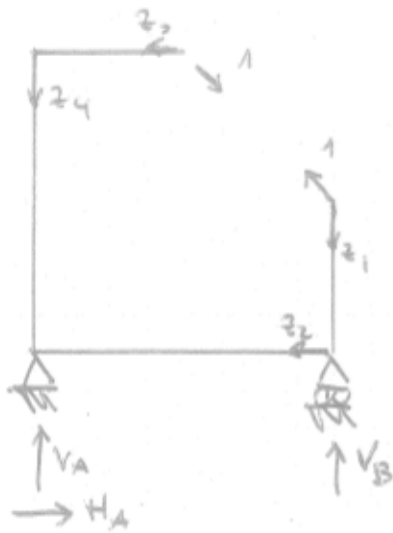
$$\begin{aligned} \rightarrow & H_A = -1 \\ \uparrow & V_B = 0 \\ \uparrow & V_A = 0 \end{aligned}$$



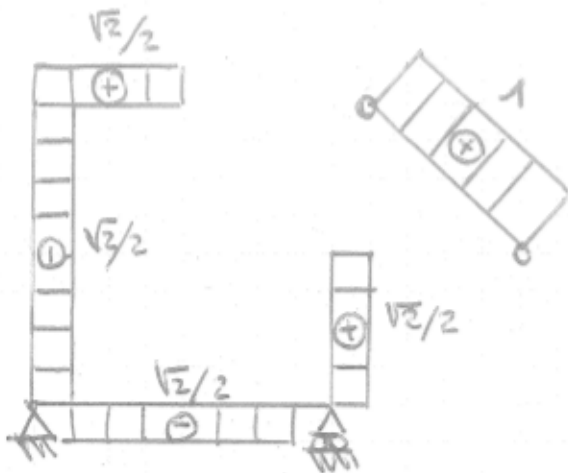
$$\begin{aligned} M_1(z_1) &= 0 \\ M_1(z_2) &= 0 \\ M_1(z_3) &= 0 \\ M_1(z_4) &= 0 \end{aligned}$$



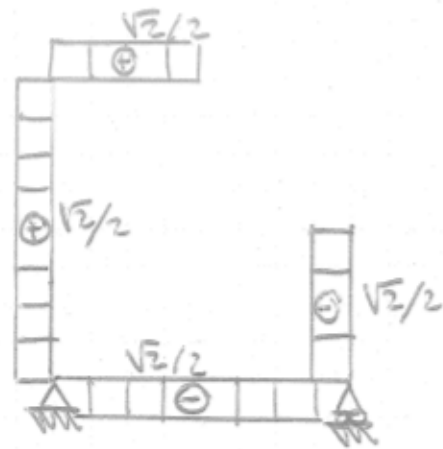
SISTEMA (2)



$$\begin{aligned} \rightarrow) H_A &= 0 \\ \uparrow) V_B &= 0 \\ \uparrow) V_A &= 0 \end{aligned}$$

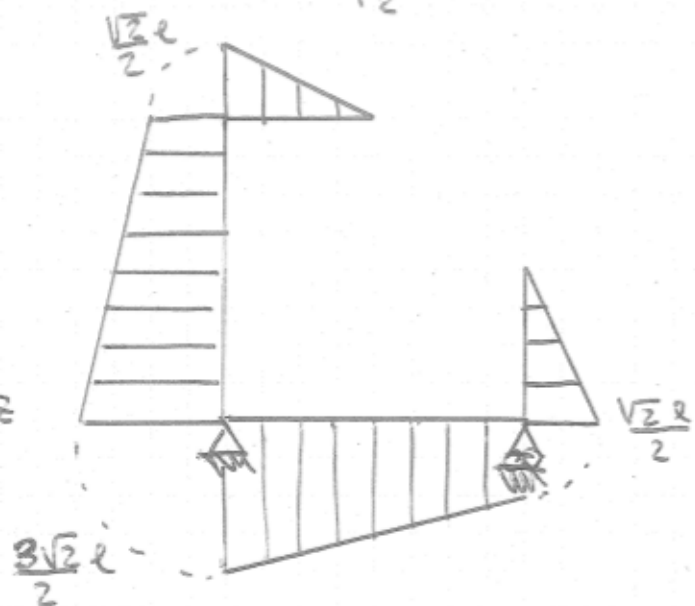


N_2



T_2

$$\begin{aligned} M_2(z_1) &= (\sqrt{2}/2) \cdot z \\ M_2(z_2) &= (\sqrt{2}l/2) + (\sqrt{2}/2) \cdot z \\ M_2(z_3) &= -(\sqrt{2}/2) \cdot z \\ M_2(z_4) &= -(\sqrt{2}l/2) - (\sqrt{2}/2) \cdot z \end{aligned}$$



$$M_{10} = 0$$

$$M_{20} = \frac{1}{EJ} \int_0^{2l} \left(\frac{\sqrt{2}}{2} (l+z) \right) (qlz) dz + \frac{1}{EJ} \int_0^{2l} \left(-\frac{\sqrt{2}}{2} (l+z) \right) \left(-\frac{qz^2}{2} \right) dz$$

$$= \frac{4\sqrt{2}}{EJ} ql^4$$

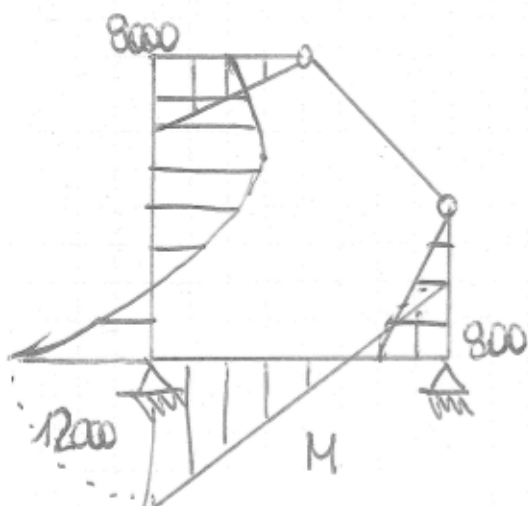
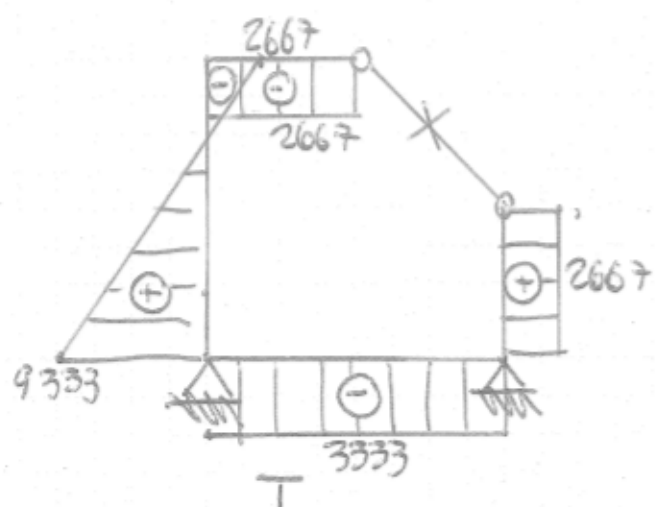
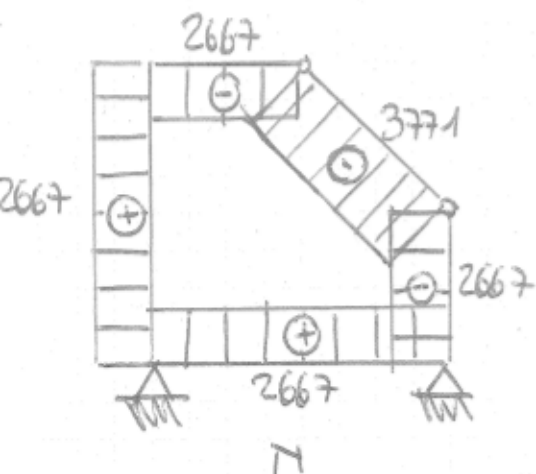
$$M_{11} = 0$$

$$M_{22} = \frac{2}{EJ} \int_0^l \left(\frac{\sqrt{2}z}{2} \right)^2 dz + \frac{2}{EJ} \int_0^{2l} \left(\frac{\sqrt{2}}{2} (l+z) \right)^2 dz = \frac{9l^3}{EJ}$$

$$M_{12} = 0$$

$$(1) \rightarrow \begin{cases} M_{11} \cdot x_1 + M_{12} \cdot x_2 = -M_{10} \\ M_{12} \cdot x_1 + M_{22} \cdot x_2 = -M_{20} \end{cases} \Rightarrow \text{IDENTITÀ} \quad \begin{matrix} \text{Poi si ha} \\ x_1 = 0 \end{matrix}$$

$$(2) \rightarrow \begin{cases} M_{11} \cdot x_1 + M_{12} \cdot x_2 = -M_{10} \\ M_{12} \cdot x_1 + M_{22} \cdot x_2 = -M_{20} \end{cases} \quad x_2 = -3771,24$$



2) PROGETTO

$$M_{max} = M_A = 12000 \text{ Nm}$$

$$N_A = 2667 \text{ N}$$

$$\sigma_{am} = 390 \text{ MPa}$$

$$W_{min} = \frac{12000 \cdot 10^3}{390} = 30769 \text{ mm}^3$$

ADOTTO IPE 120

$$W_x = 52,96 \text{ cm}^3 \quad J_x = 317,8 \text{ cm}^4 \quad A = 13,21 \text{ cm}^2$$

$$E = 210000 \text{ MPa}$$

$$\sigma_{max} = \frac{N}{A} + \frac{M_{max}}{W} = \frac{2667}{13,21 \cdot 10^{-2}} + \frac{12000 \cdot 10^3}{52,96 \cdot 10^3} = 228,61 < 390 \text{ ok!}$$

$$3) M_{11}^N = \frac{1}{EA} \int_0^{2l} (1)^2 dz = \frac{2l}{EA}$$

$$M_{22}^N = \frac{6}{EA} \int_0^l \left(\frac{\sqrt{2}}{2}\right)^2 dz + \frac{1}{EA} \int_0^{\sqrt{2}l} (1)^2 dz = \frac{(3+\sqrt{2})l}{EA}$$

$$M_{12}^N = \frac{1}{EA} \int_0^{2l} (1) \left(-\frac{\sqrt{2}}{2}\right) dz = -\frac{\sqrt{2}l}{EA}$$

$$M_{ij}^{TOT} = M_{ij}^{\dot{\cdot}} + M_{ij}^{\ddot{\cdot}} N$$

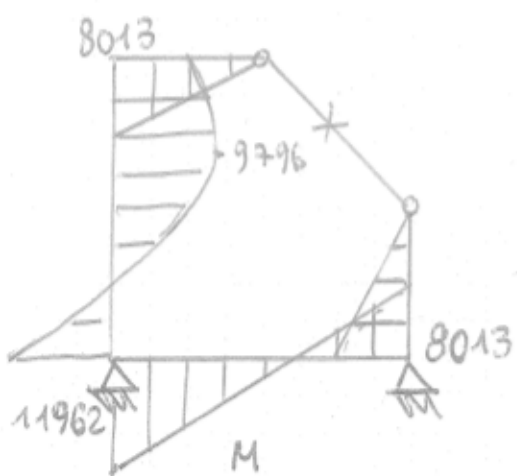
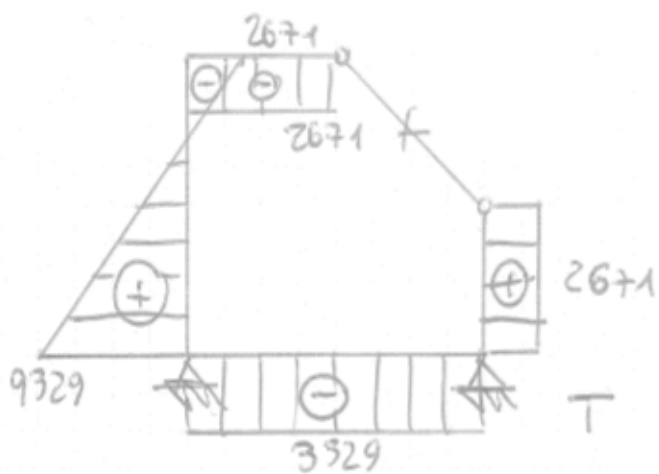
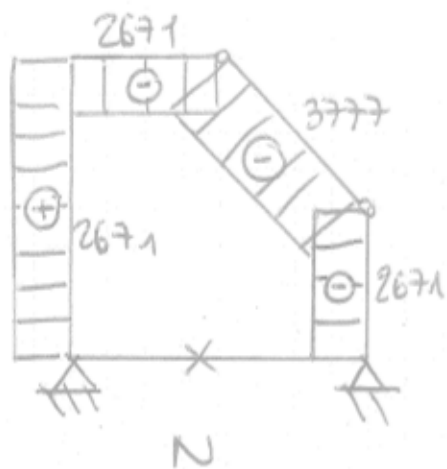
$$\alpha = 1,2 \cdot 10^{-5} \quad \Delta t = 30^\circ \quad \epsilon^* = \alpha \Delta t$$

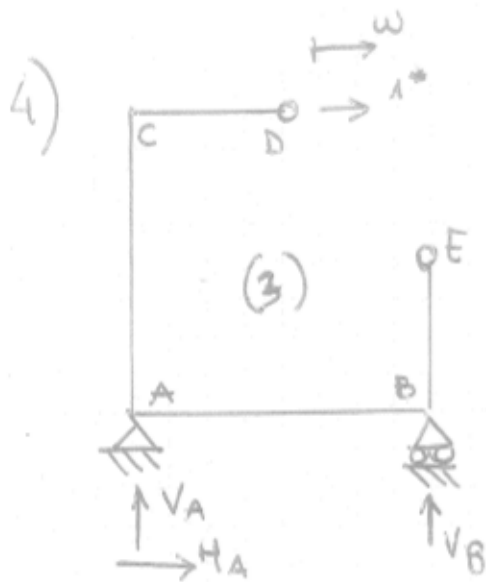
$$(1) \rightarrow \begin{cases} M_{11}^{TOT} \cdot x_1 + M_{12} \cdot x_2 + M_{10} \end{cases}$$

$$(2) \rightarrow \begin{cases} M_{12} \cdot x_1 + M_{22} \cdot x_2 + M_{20} + \int_0^{\sqrt{2}l} (1) \cdot \alpha \Delta t dz = 0 \end{cases}$$

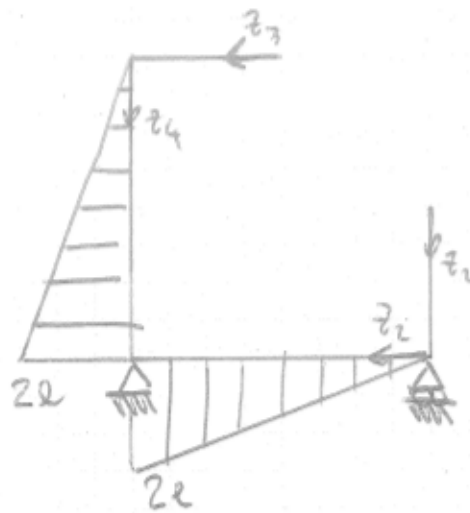
$$x_1 = 2670,85 \text{ N}$$

$$x_2 = 3777,15 \text{ N}$$





$$\begin{aligned} \rightarrow) H_A &= -1 \\ \uparrow) V_B &= 1 \\ \uparrow) V_A &= -1 \end{aligned}$$



$$\begin{aligned} M_3(z_1) &= 0 \\ M_3(z_2) &= z \\ M_3(z_3) &= 0 \\ M_3(z_4) &= -z \end{aligned}$$

Utilizzando X_1 e X_2 del punto 3

$$\begin{aligned} 1^* \cdot w &= \frac{1}{EI} \int_0^{2l} (z) (qlz) dz + \frac{1}{EI} \int_0^{2l} (-z) \left(-\frac{qz^2}{2}\right) dz + X_1 \begin{bmatrix} 0 \end{bmatrix} + \\ &+ X_2 \left[\frac{2}{EI} \int_0^l (z) \left(\frac{\sqrt{2}}{2} (l+z)\right) dz \right] = 0,1247 \text{ m} \end{aligned}$$